

DE LA RECHERCHE À L'INDUSTRIE



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Electromechanical modelling of fusion cables

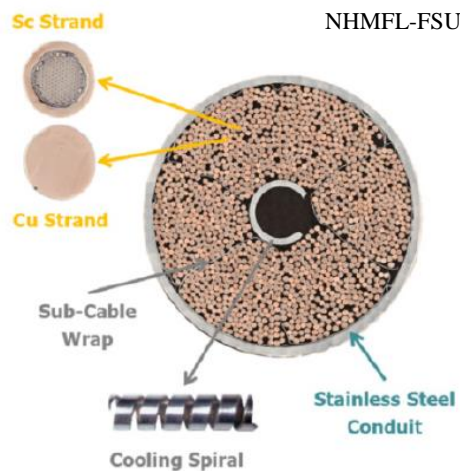
Presenter: Rebecca Riccioli
20/09/2021



Co-authors:

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Marco Breschi	(UNIBO-LIMSA)
Damien Durville	(ECS-MSSMat)
Frédéric Lebon	(AMU-LMA)

Superconducting conductors for tokamaks: Cable-In-Conduit Conductors (CICCs)



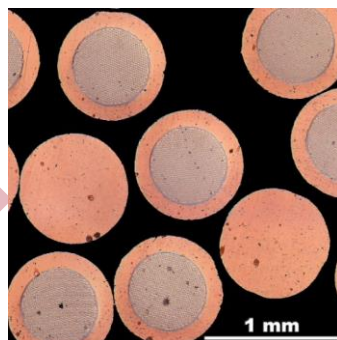
NHMFL-FSU



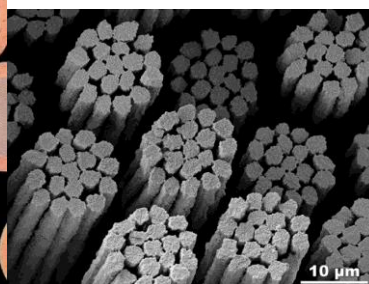
ITER TF CICCs

Taken from: A. Devred *et al* 2014 *Supercond. Sci. Technol.* 27 044001

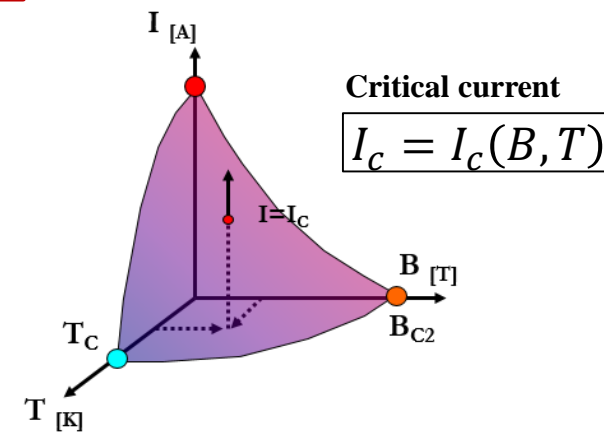
Composite Nb_3Sn wire



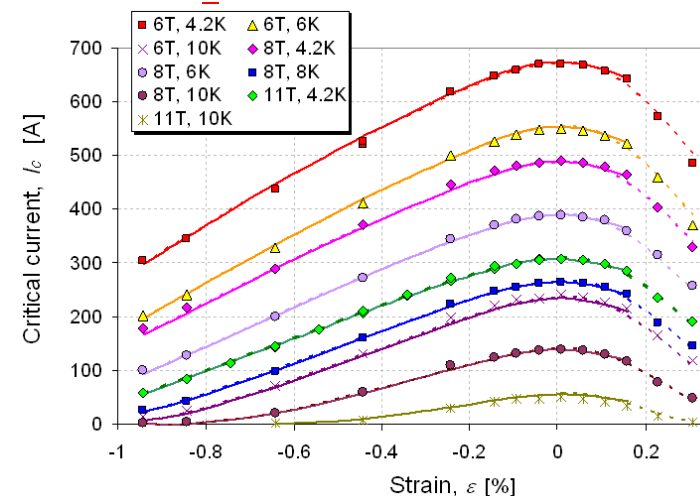
Micro-filaments



Images of P. Lee & C. Sanabria from NHMFL-FSU



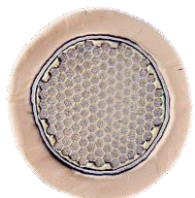
For Nb_3Sn wires $I_c = I_c(B, T, \varepsilon)$



Taken from: Y. Ilyin *et al* 2007 *Supercond. Sci. Technol.* 20 186

Scaling up from strand to cable ?

Nb₃Sn wire

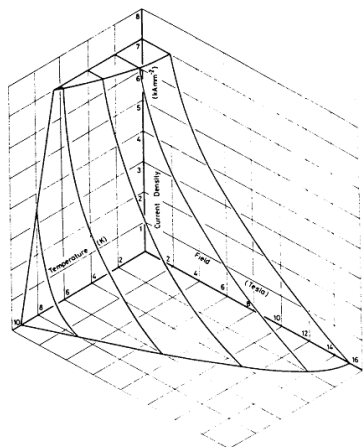


P. Lee & C. Sanabria
(NHMFL-FSU)

CIC Conductor



P. Lee & C. Sanabria
(NHMFL-FSU)



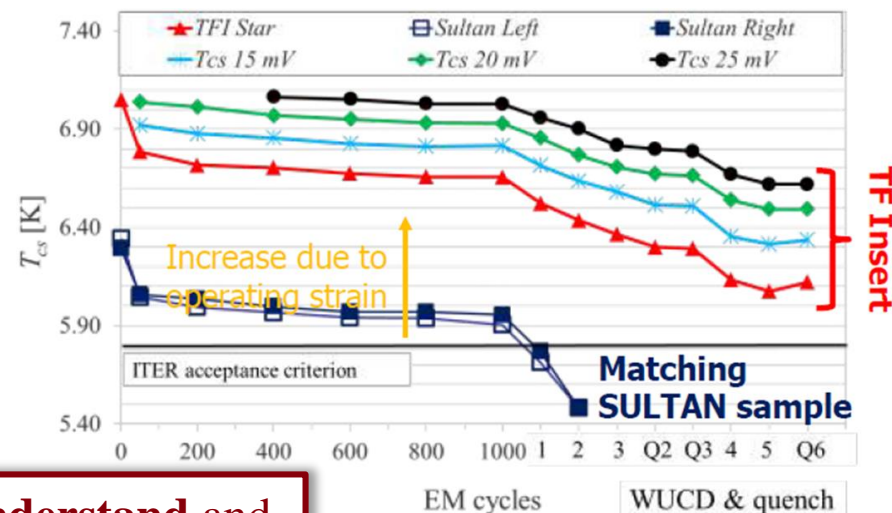
Taken from: M. N. Wilson, *Oxford Science Publications*, 1993

Need for a tool able to understand and predict the electrical performance of a superconducting fusion cable

Performance degradation ?

ITER TF CICC's cyclic mechanical loadings due to:

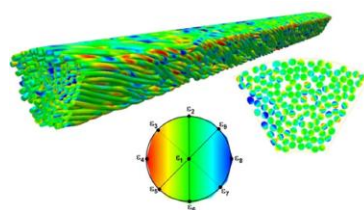
- **Cool-down** after manufacturing (923.15 K to 4.5 K)
- **Warm-up-cool-down** during operation [~ 50-100 cycles]
- **Electromagnetic cycles** [~ 1000]
→ Lorentz force (68 kA, 11.78 T) ~ 80 t/m



TF Insert

2011

H. Bajas Ph.D.



Development of a first mechanical model to simulate fusion sub-cables based on MULTIFIL code developed by D. Durville:

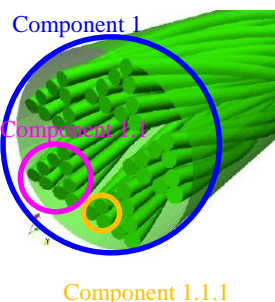
- Material constitutive laws implementation;
- Axial and transverse validation;
- Deep analysis of the ITER CS CICC and main mechanical phenomena.

But missing numerical tools and phenomena: representability ?

2017

MULTIFIL upgrade

Passage from pseudo-periodic BCs to **hierarchical handling of BCs**:
Independency of the ends BCs

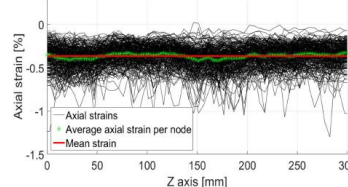


2019

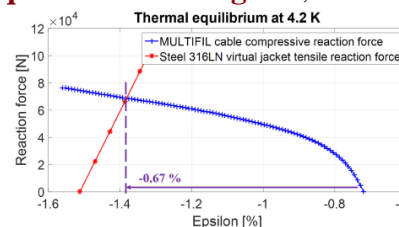
MULTIFIL upgrade & Model improvement

Further developments of the single sub-cable model:

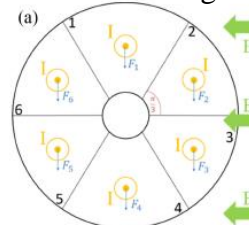
- MULTIFIL upgrade: deformable “jacket” during CD;



- **Jacket-cable thermal equilibrium during CD;**



- “Multi-petal” models during EM cycles.



2020

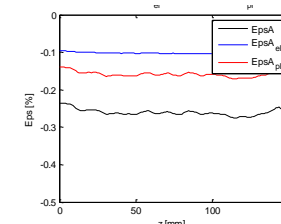
MULTIFIL upgrade & Model improvement

MULTIFIL upgrades:

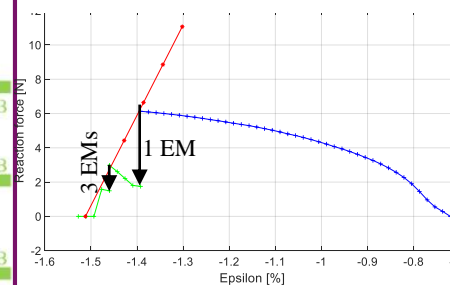
- **Twisted single sub-cable;**



- Discrimination between plastic and elastic strains over strands;



Adding the **jacket-cable equilibrium for EM cycles.**



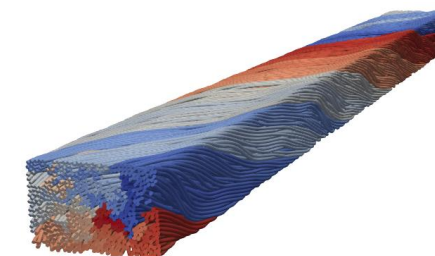
2021

MULTIFIL upgrade & new models

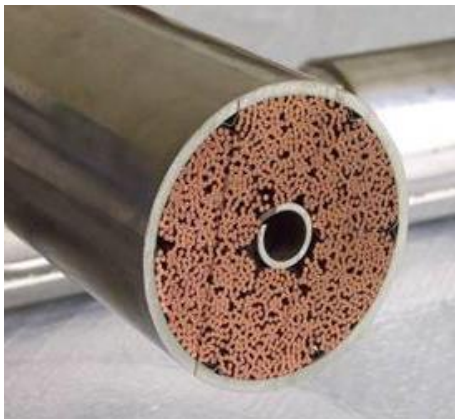
- MULTIFIL upgrade: **full ITER TF CICC simulation;**



- **Other Nb₃Sn cables simulation:** DTT TF cable, JT60SA CS cable, ITER CS STP cable.



MULTIFIL allows to simulate the main phases of the conductor life starting from the manufacturing, which is here the global shaping of the strands assembly.

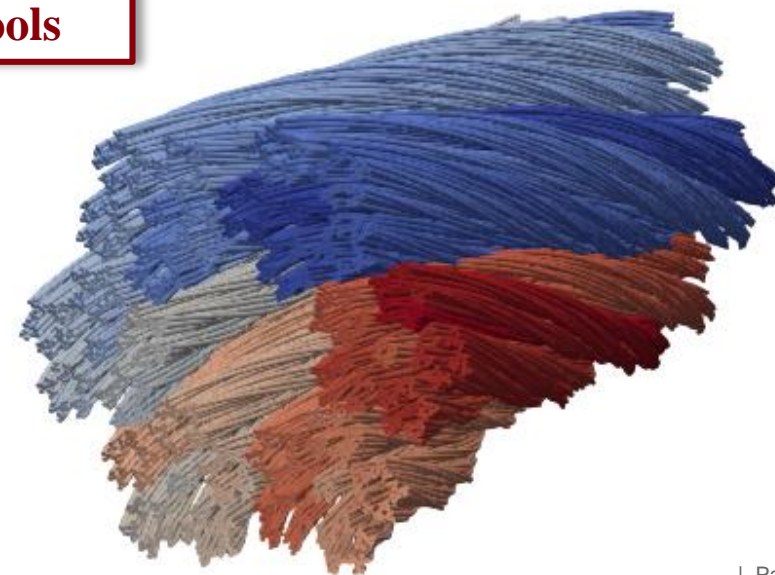
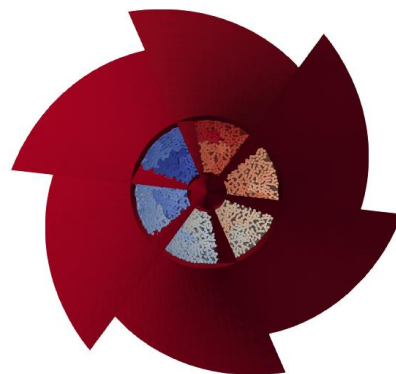
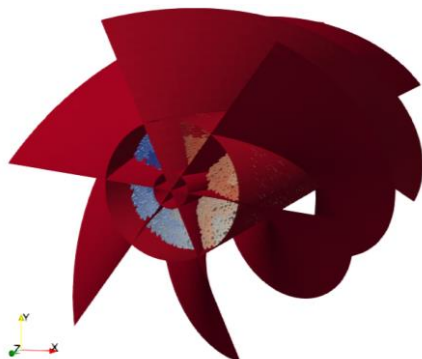


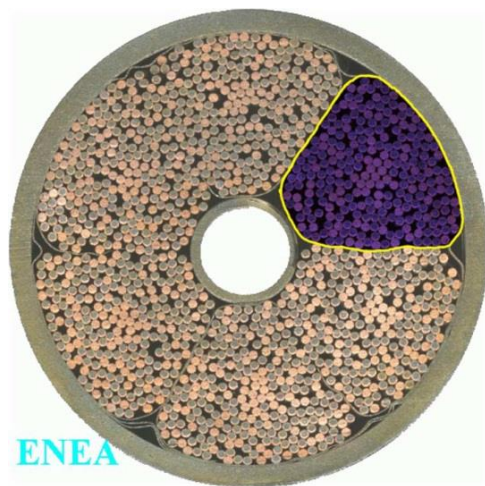
Taken from: M. Breschi *et al* 2017
Supercond. Sci. Technol. 30 055007

$$6 \times [(2\text{Nb}_3\text{Sn} + 1\text{Cu}) \times 3 \times 5 \times 5 + (3\text{Cu}) \times 4]$$

The initial shape is given by the compaction of strands that follow superposed helical trajectories. For each cabling stage, an helix is defined and the result is the superposition of five helices.

The initial trajectories are the result of the compaction by rigid tools





ENEA

Design:

$$\cos\vartheta = 0.97$$

$$VF = 29.7 \%$$

$$\text{Diam} = 39.7 \text{ mm}$$

Scaling up of the ITER TF CICC model

Straight Petal (SP)



$$\cos\vartheta = 0.988$$

$$\text{Diam} = 38.44 \text{ mm}$$

$$VF = 29.7 \%$$

$$\text{Length} = 300 \text{ mm}$$

STRAIGHT PETAL

Twisted Petal (TP)



$$\cos\vartheta = 0.968$$

$$\text{Diam} = 38.8 \text{ mm}$$

$$VF = 29.7 \%$$

$$\text{Length} = 300 \text{ mm}$$

TWISTED PETAL

Full Cable (FC)



$$\cos\vartheta = 0.967$$

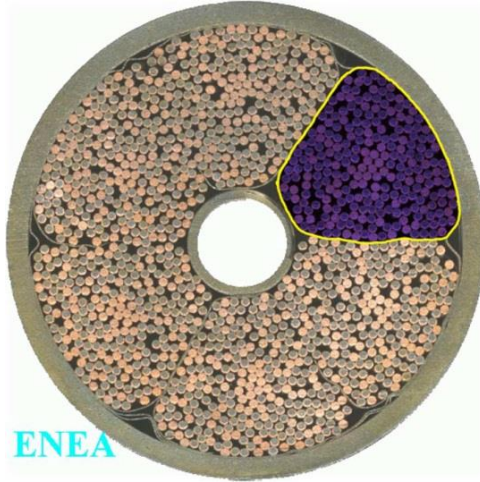
$$\text{Diam} = 38.86 \text{ mm}$$

$$VF = 29.8 \%$$

$$\text{Length} = 150 \text{ mm}$$

FULL CABLE

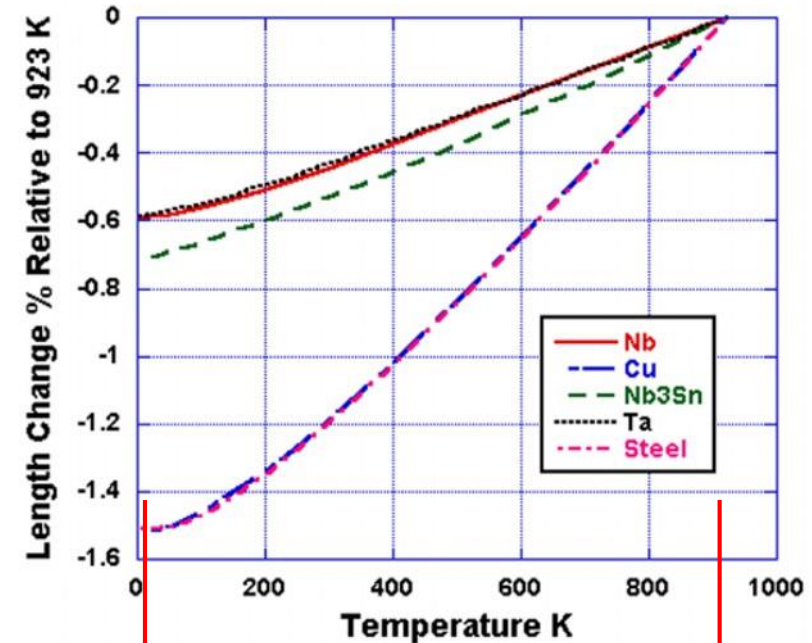
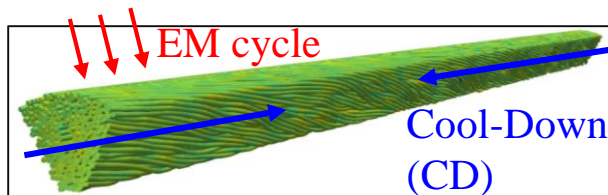
After shaping the other critical phases of the conductor life are the Cool-Down (CD) and the EM loadings.



Steel and Nb₃Sn wires
have different coefficients
of thermal expansion
(contraction in this case)



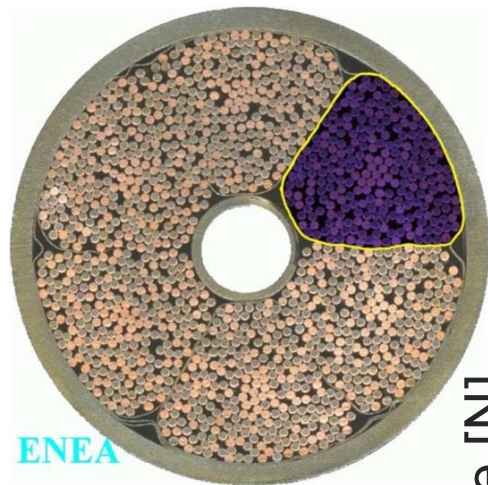
The cable work in a global state of
compression inside the conductor



Operating
temperature

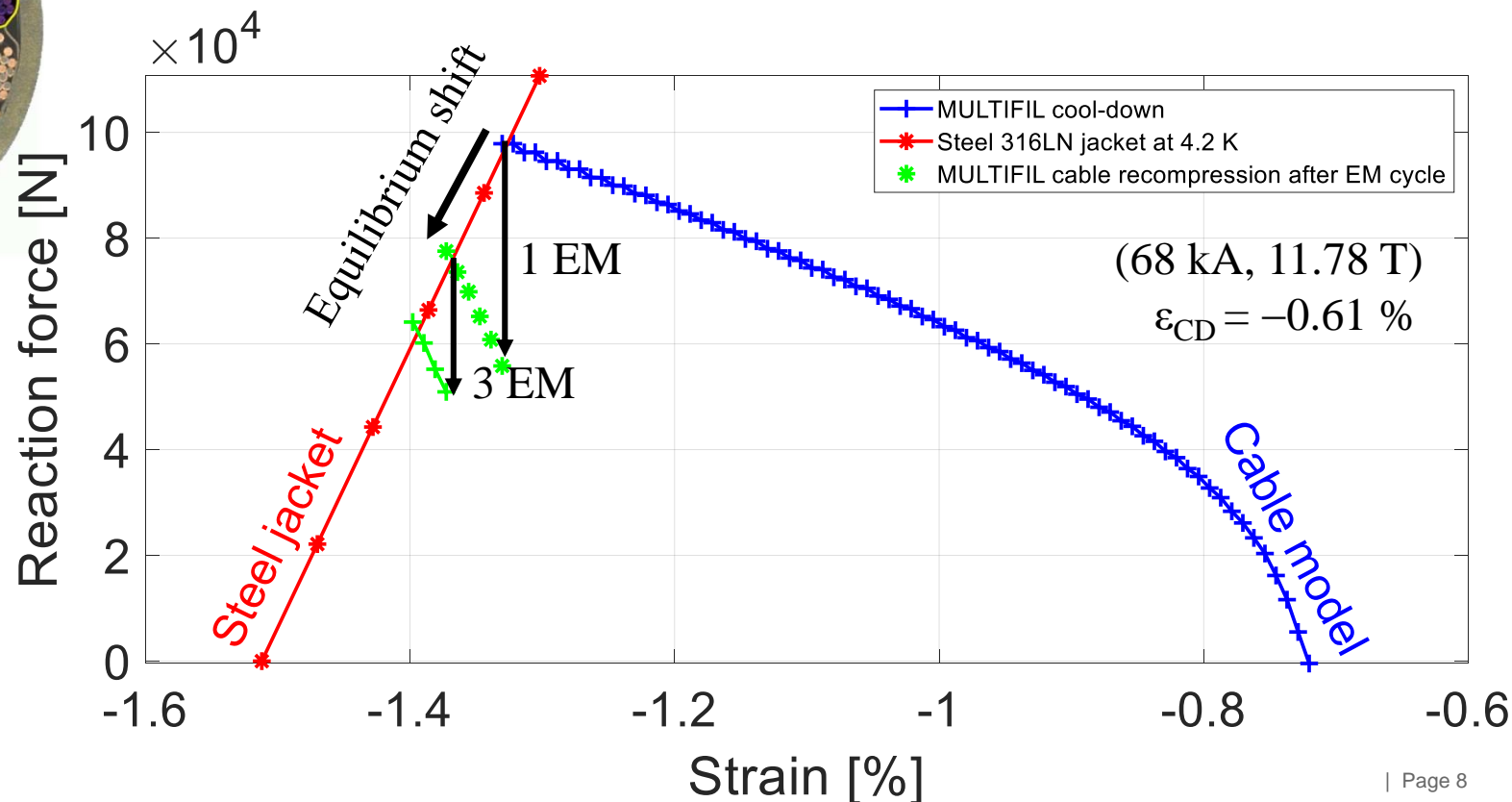
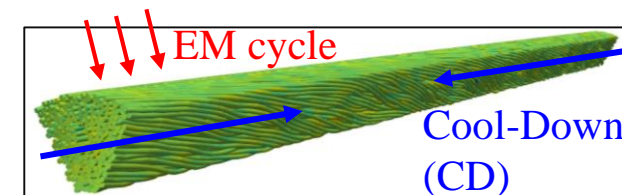
Heat treatment
temperature

After shaping the other critical phases of the conductor life are the Cool-Down (CD) and the EM loadings.



ENEA

**Gradual compressive shifts of
jacket-cable equilibrium due
to EM load**



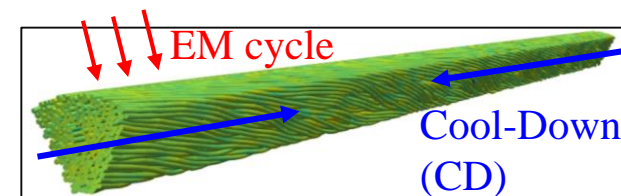
**The model
considers the
presence of the
jacket even if it is
not simulated**

Straight Petal (SP)

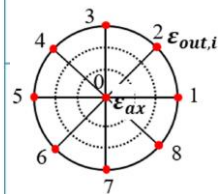
$\cos\theta = 0.988$
Diam = 38.44 mm
VF = 29.7 %
Length = 300 mm
STRAIGHT PETAL

(68 kA, 11.78 T)

$\varepsilon_{CD} = -0.61 \%$



**New identified
phenomenon: plastic
softening due to EM load**



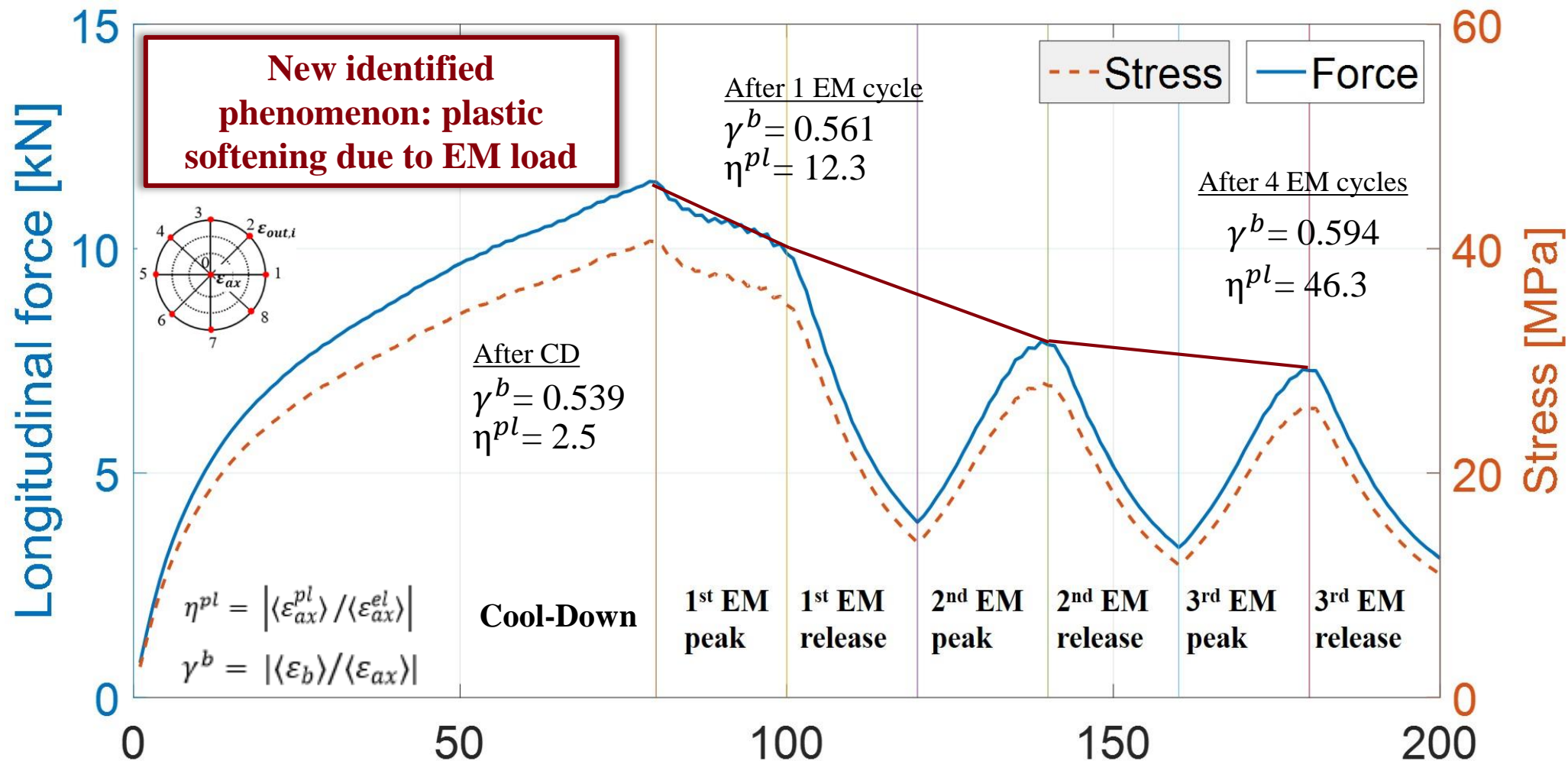
$$\eta^{pl} = \left| \frac{\langle \varepsilon_{ax}^{pl} \rangle}{\langle \varepsilon_{ax}^{el} \rangle} \right|$$

$$\gamma^b = \left| \frac{\langle \varepsilon_b \rangle}{\langle \varepsilon_{ax} \rangle} \right|$$

After CD
 $\gamma^b = 0.539$
 $\eta^{pl} = 2.5$

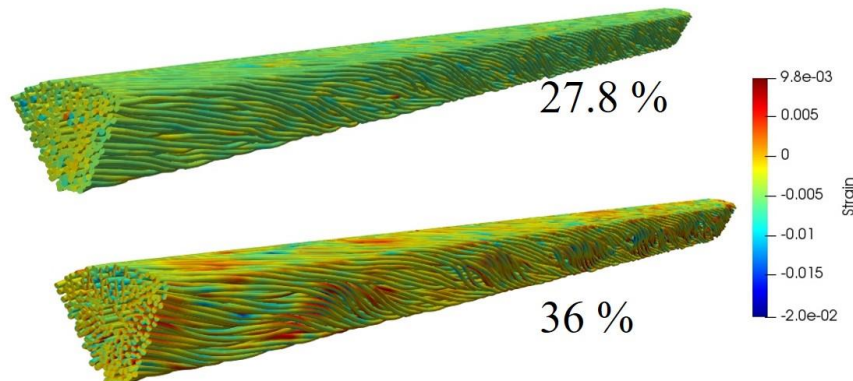
After 1 EM cycle
 $\gamma^b = 0.561$
 $\eta^{pl} = 12.3$

After 4 EM cycles
 $\gamma^b = 0.594$
 $\eta^{pl} = 46.3$

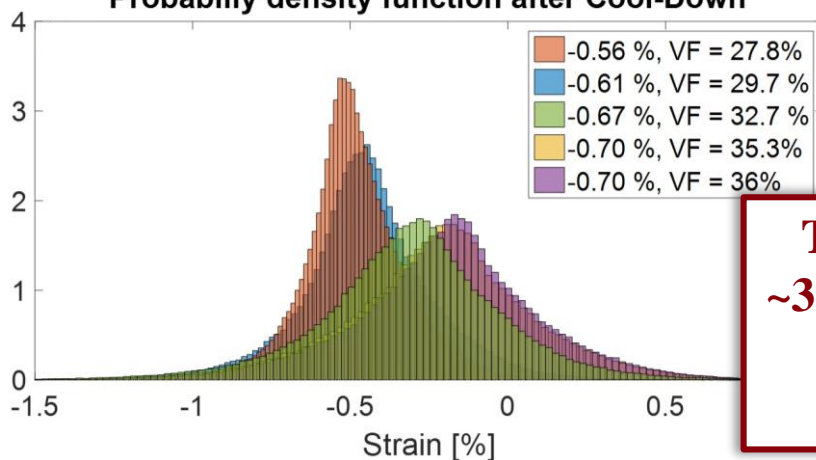


Straight Petal (SP)

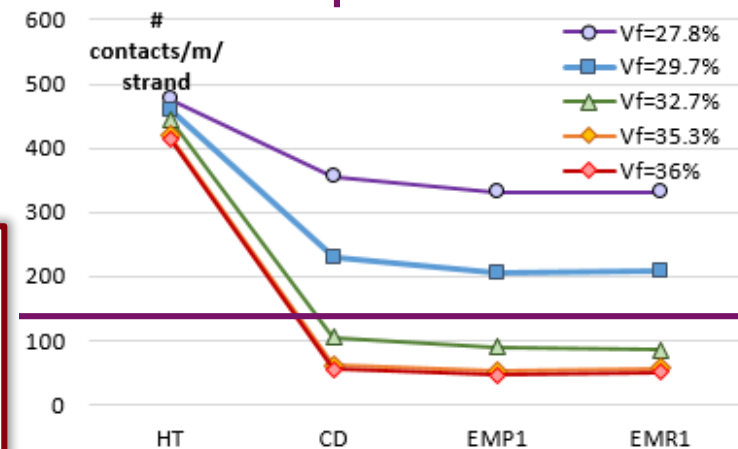
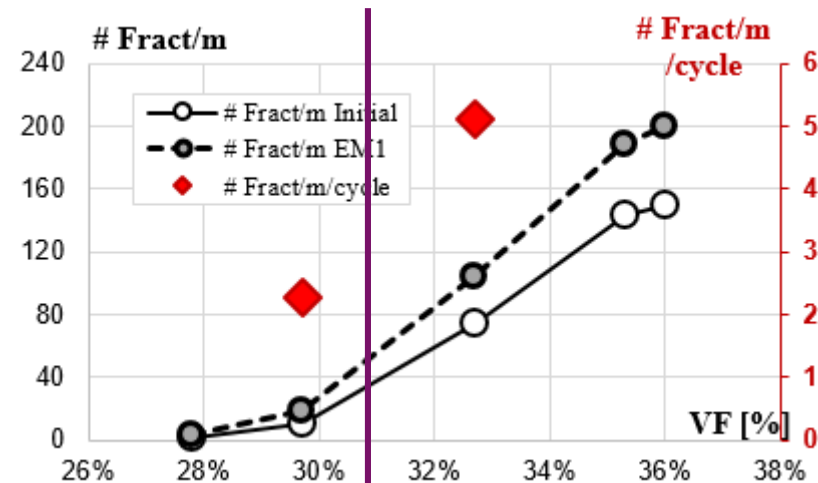
$\cos\theta = 0.988$
Diam = 38.44 mm
VF = 29.7 %
Length = 300 mm
STRAIGHT PETAL



Probability density function after Cool-Down



Mechanical exposure to fracture as a function of the VF



**Threshold around
~31 % of VF between
locked and loose
behavior.**

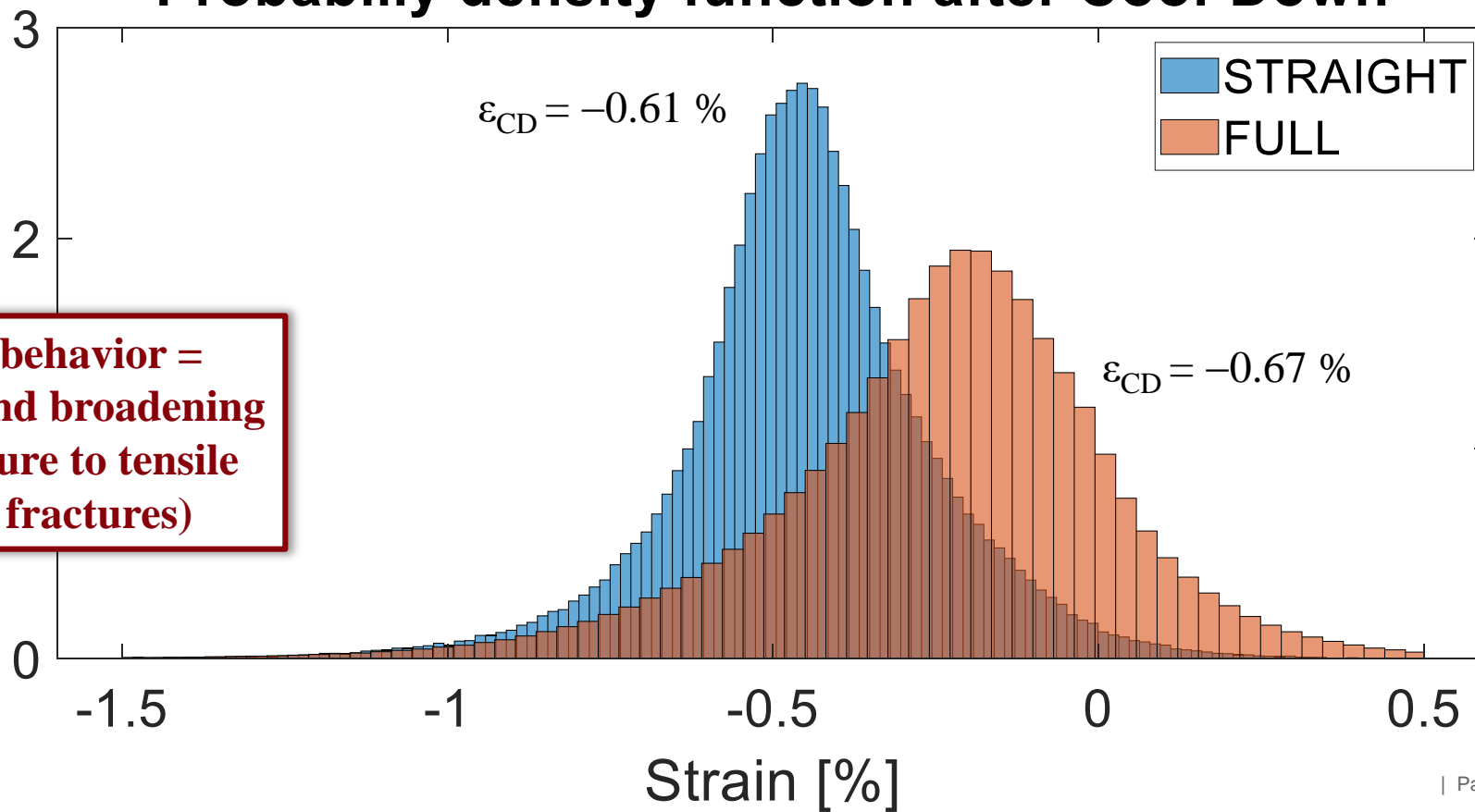
Full Cable (FC)



$\cos\theta = 0.967$
Diam = 38.86 mm
VF = 29.8 %
Length = 150 mm
FULL CABLE

Full model VS Petal model mechanical comparison ?

Probability density function after Cool-Down



**Full cable behavior =
tensile shift and broadening
(more exposure to tensile
strains → fractures)**

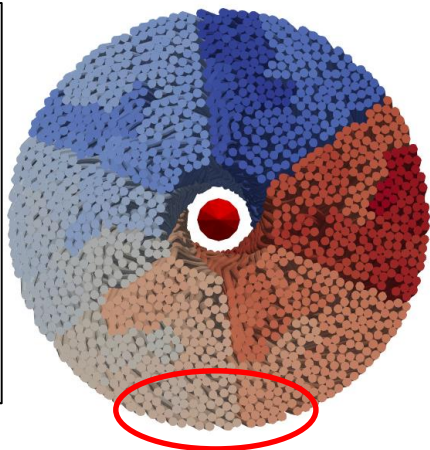
Full Cable (FC)



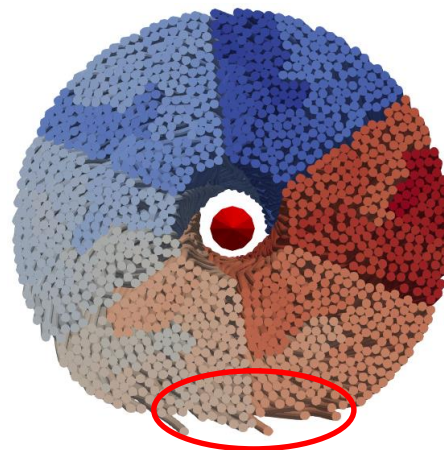
$\cos\theta = 0.967$
Diam = 38.86 mm
VF = 29.8 %
Length = 150 mm
FULL CABLE

The full cable model shows a large displacement of the wires during the EM cycle in the low pressure side

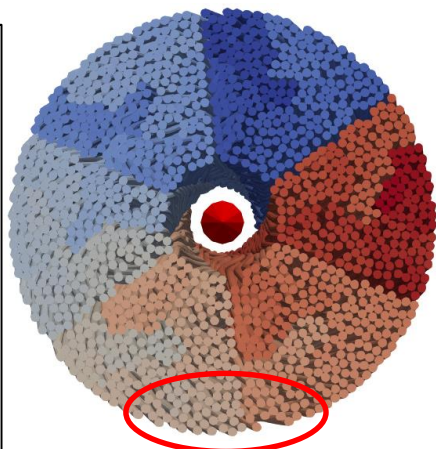
Before EM cycle



Peak EM cycle



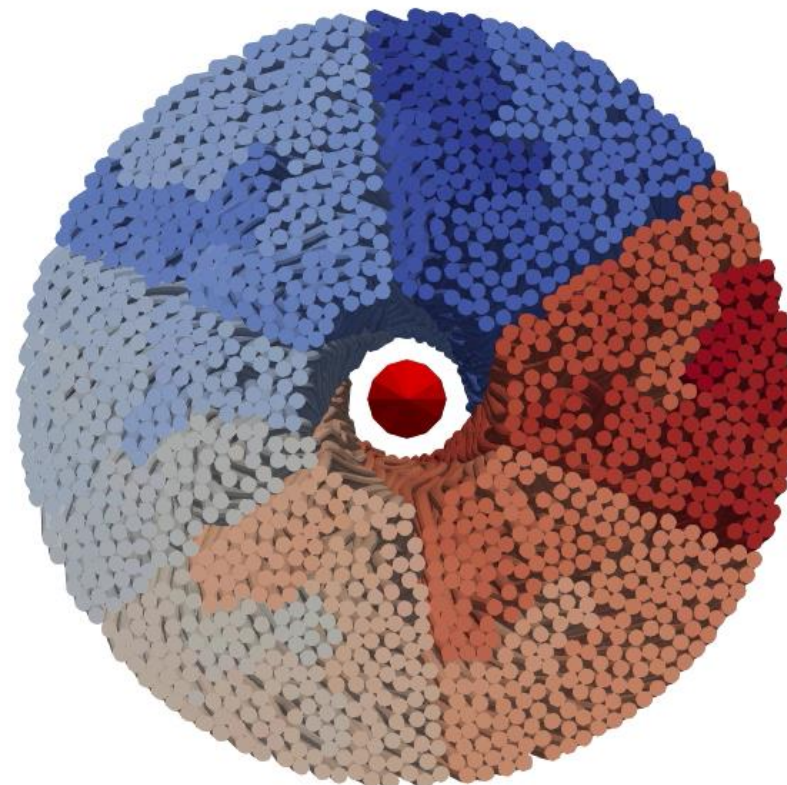
Release EM cycle



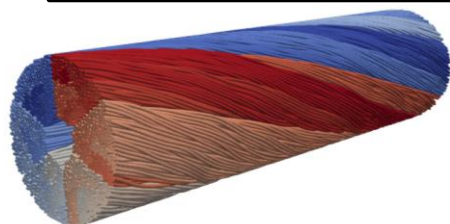
$I \times B$



(68 kA, 11.78 T)
 $\epsilon_{CD} = -0.67 \%$



Full Cable (FC)



The local twist angle shows a radial gradient

The VF increases in the low pressure zone due to the application of the EM cycle

The strong contacts tend to disappear in the low pressure side

$\cos\theta = 0.967$
Diam = 38.86 mm
VF = 29.8 %
Length = 150 mm
FULL CABLE

Local $\cos\theta$

Local VF

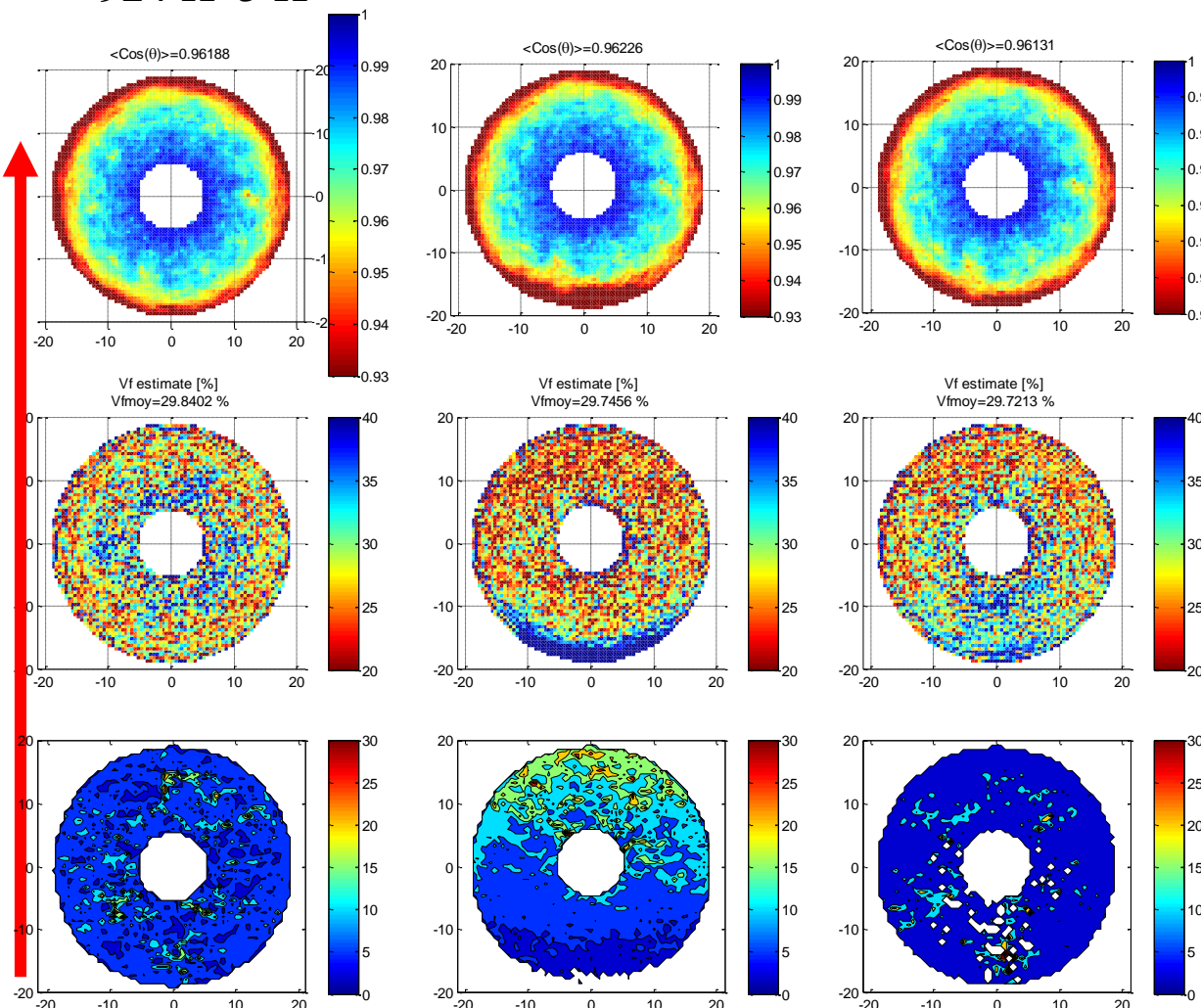
Contact forces

Cool-Down
924 K–5 K

EM peak
(68 kA, 11.78 T)

EM release

$I \times B$



Full Cable (FC)



$\cos\theta = 0.967$
Diam = 38.86 mm
VF = 29.8 %
Length = 150 mm
FULL CABLE

Metallographic autopsies of full-scale ITER prototype cable-in-conduit conductors after full cyclic testing in SULTAN: III. The importance of strand surface roughness in long twist pitch conductors

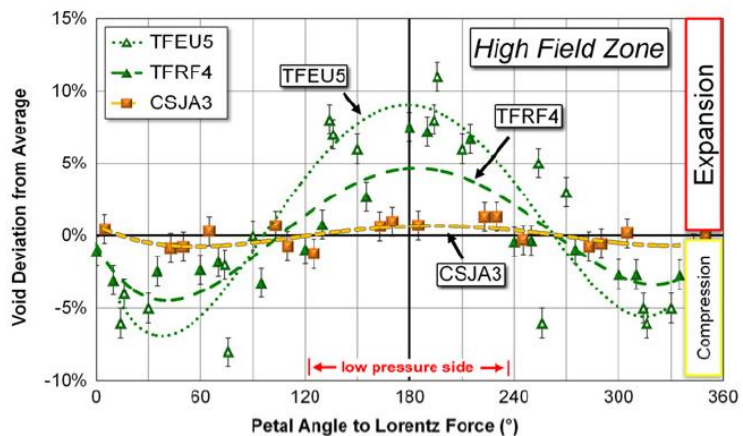
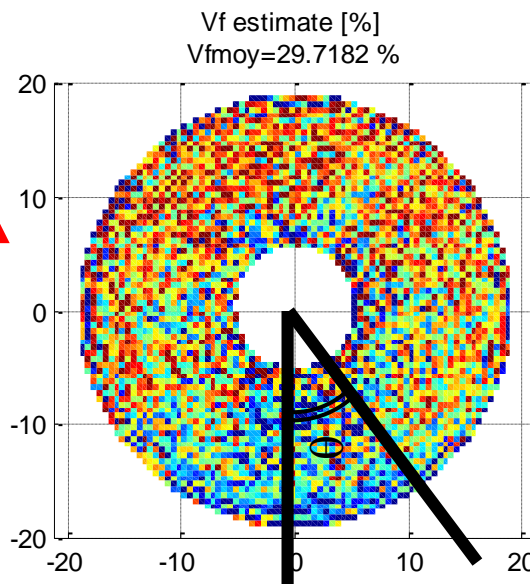
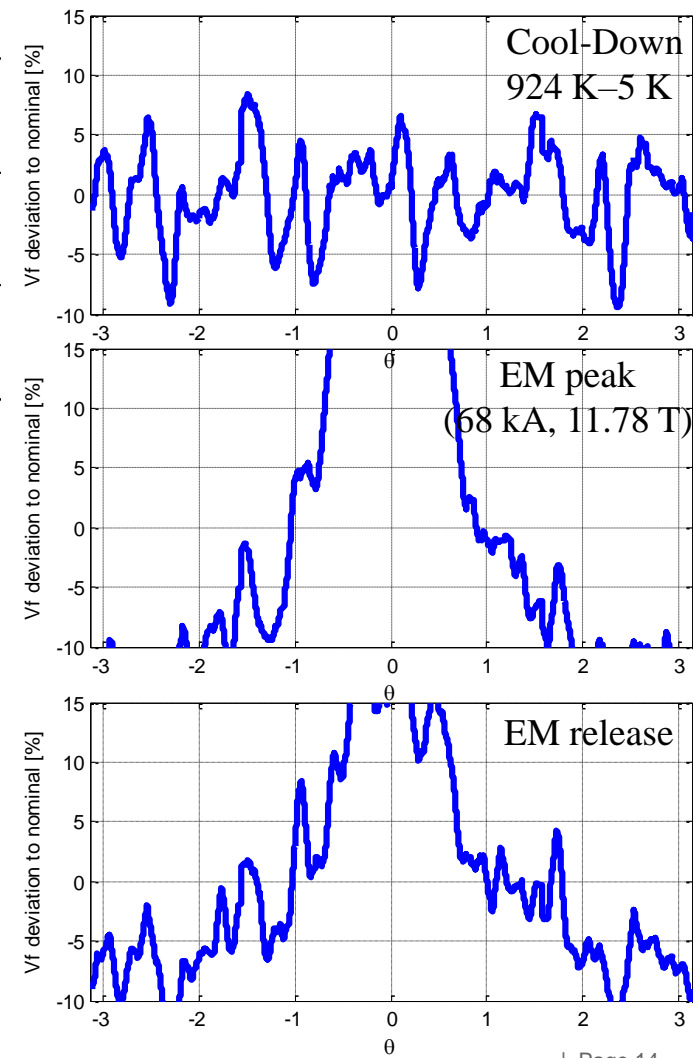


Figure 5. Petal void fraction expansion or compression (from the average of all petals) as a function of petal position which is defined with respect to the Lorentz force. 0° defines the high pressure side of maximum Lorentz force while petals in the vicinity of 180° lie on the low pressure side.

$I \times B$



The local VF deviation from average value as a function of the angular position shows very good agreement with the experimental measurements



Full Cable (FC)



$\cos\theta = 0.967$
Diam = 38.86 mm
VF = 29.8 %
Length = 150 mm
FULL CABLE

Axial strain

Plastic axial strain

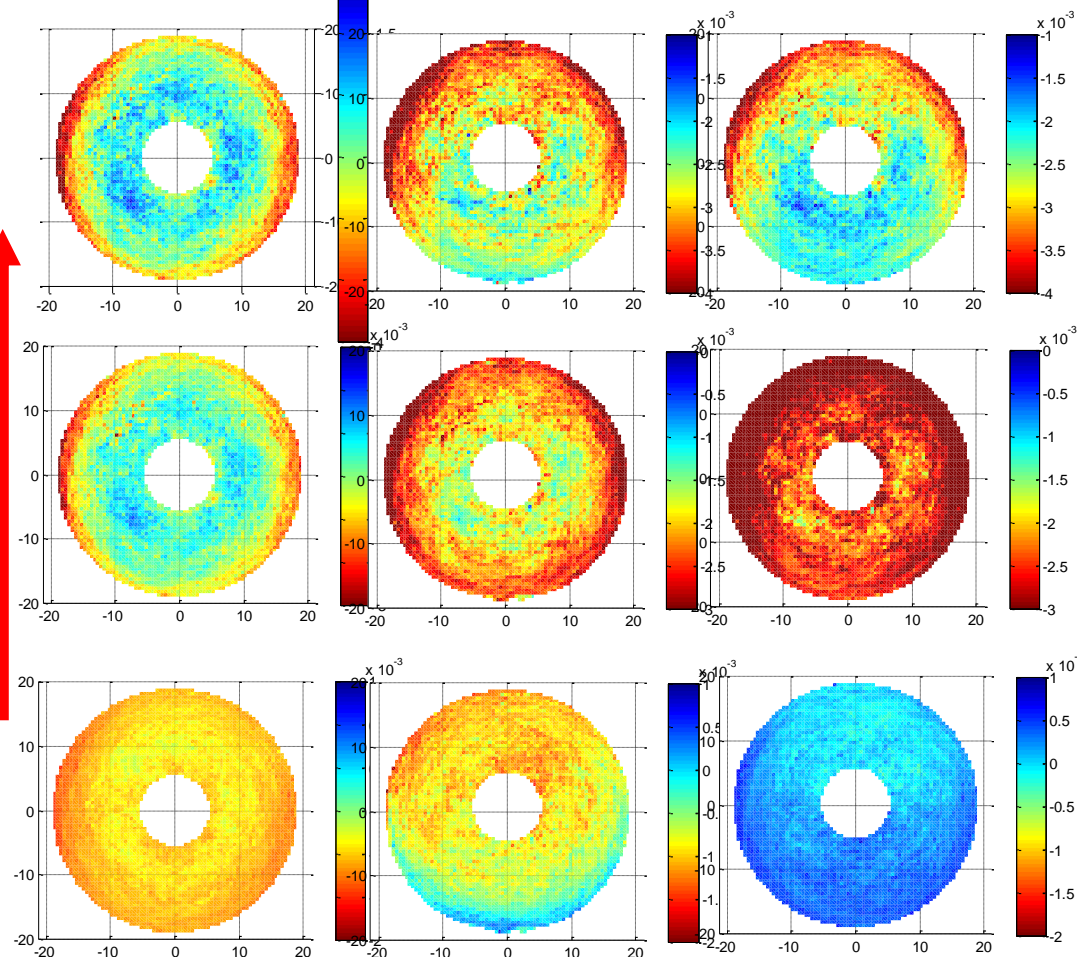
Elastic axial strain

$I \times B$

Cool-Down
924 K–5 K

EM peak
(68 kA, 11.78 T)

EM release



The major effect of the EM cycle is a global plasticization of the strain with major localization in the low pressure side of the cable

Full Cable (FC)



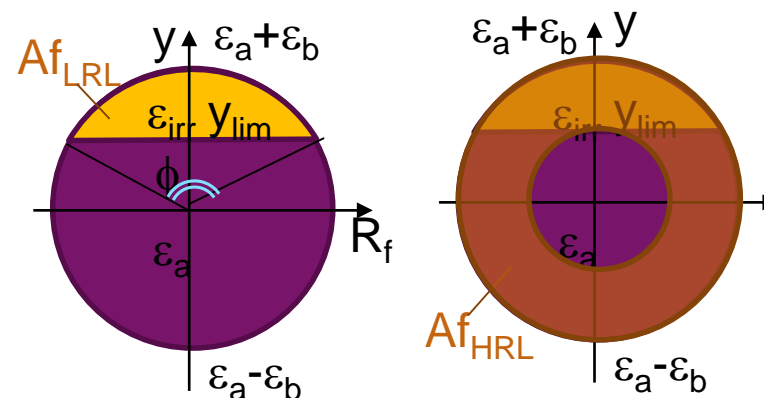
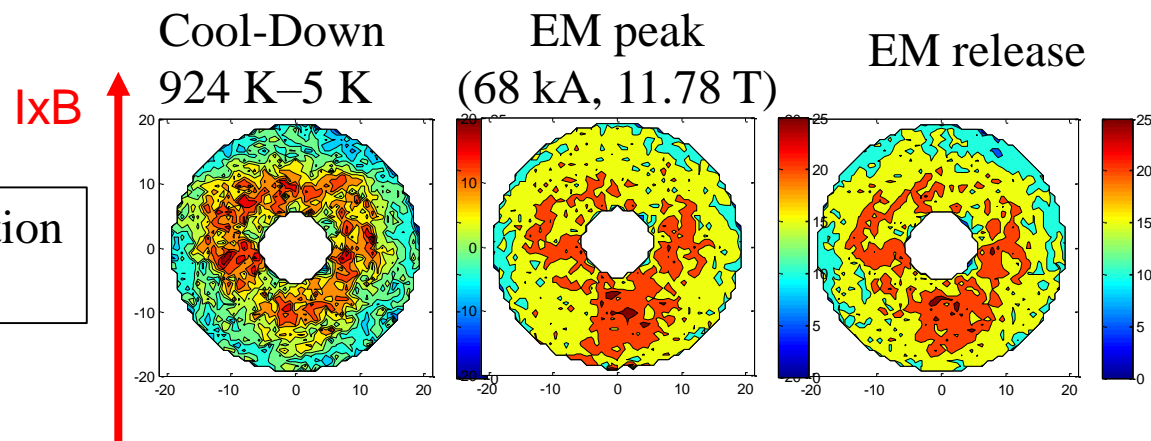
$\cos\theta = 0.967$
Diam = 38.86 mm
VF = 29.8 %
Length = 150 mm
FULL CABLE

Surface fraction
at $\varepsilon > 0$ %

The low pressure side is characterized
by more exposure to fractures and so
stronger decrease of I_c .

Breakage models:

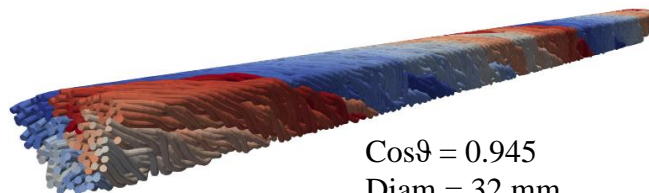
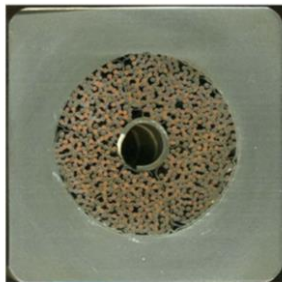
- Low Resistivity Limit: - 10 % I_c
- High Resistivity Limit: - 20 % I_c



ITER CS STP

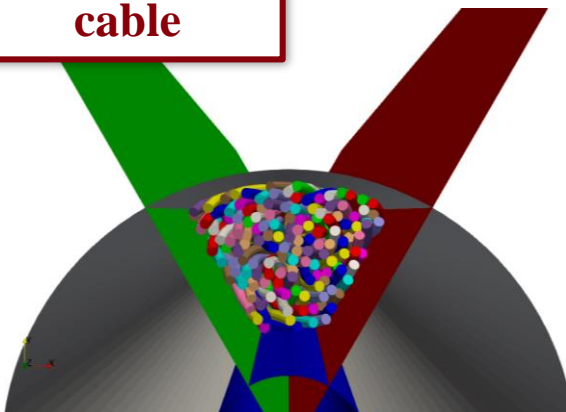
Design:

$\cos\theta = 0.945$
VF = 33 %
Diam = 32.6 mm



$\cos\theta = 0.945$
Diam = 32 mm
VF = 33.5 %
Length = 300 mm
STP
STRAIGHT PETAL

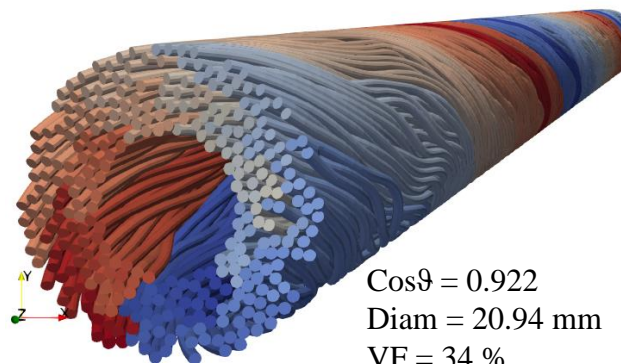
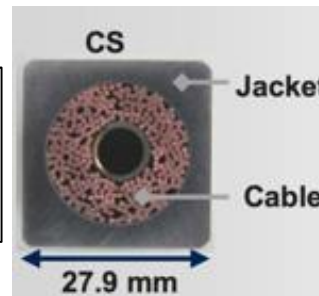
**Ready for
the scaling-
up to full
cable**



JT60SA CS

Design:

$\cos\theta = ?$
VF = 34 %
Diam = 21 mm



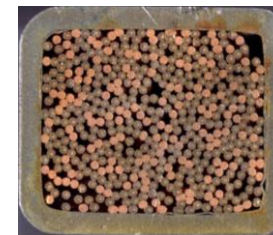
$\cos\theta = 0.922$
Diam = 20.94 mm
VF = 34 %
Length = 300 mm
FULL CABLE



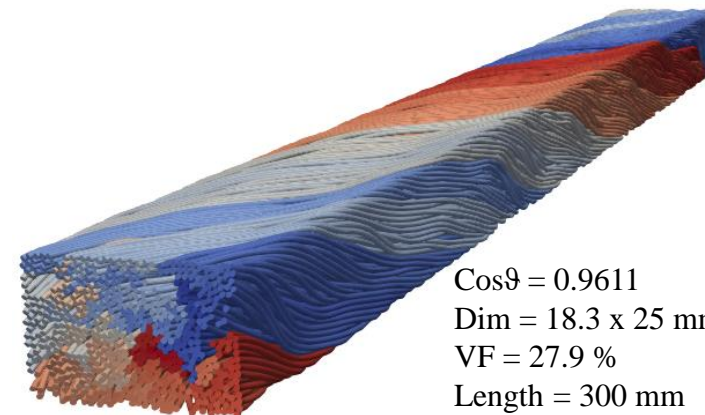
DTT TF

Design DTT:

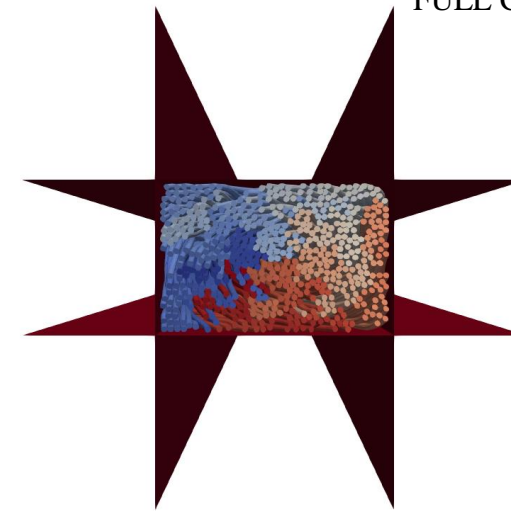
$\cos\theta = ?$
VF = 26.4 %
Dim = 18.3 x 25 mm



Picture of JT60SA TFSL



$\cos\theta = 0.9611$
Dim = 18.3 x 25 mm
VF = 27.9 %
Length = 300 mm
FULL CABLE



**Thank you for
your attention !**

Questions ??