

DE LA RECHERCHE À L'INDUSTRIE

Dynamic simulation of high transients in a forced flow Supercritical helium loop for the sizing of an experimental set-up dedicated to the study of loss of vacuum

21th september 2021

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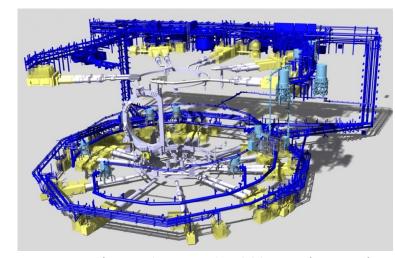


Safety in cryogenics

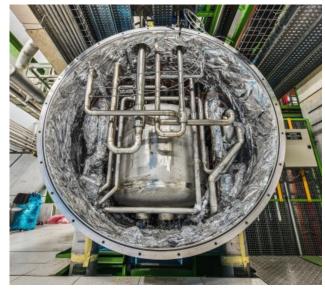
- ► Insulating vacuum failure is a major accident scenario
 - Large break on the Cryostat
 - Outside atmospheric air rushes into the vacuum space and condenses on cold surfaces
 - Very high heat load transferred to the cryogenic fluid
- Cryogenics devices have to be protected against overpressure
 - By using safety valves or rupture disks
- ► For instance, safety relief devices are sized by using a constant heat flux value :
 - Helium tank in diphasic discharge, without insulation: 3.8W/cm²
 - Helium tank in supercritical discharge, without insulation: 2W/cm²
- ► Reference values of heat flux have just been measured for tank

Question: Which value of heat flux has to be considered for supercritical helium flowing in pipe?

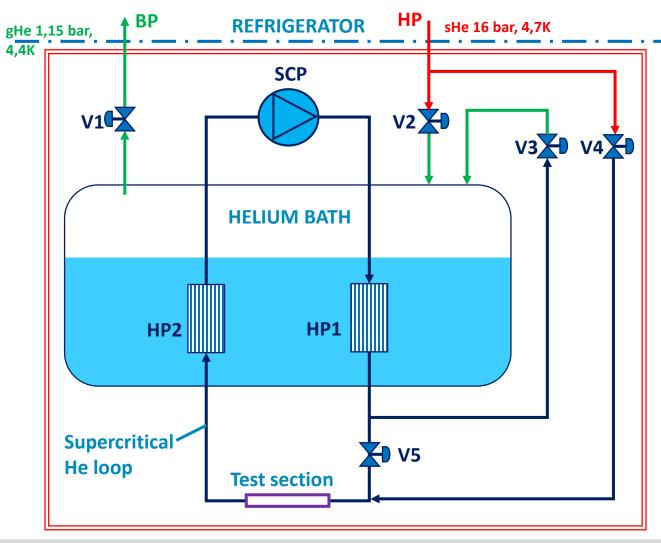
Objective: Develop an experimental device to perform experimental measure of the heat flux



Iter's Cryolines and cold boxes (iter.org)



CERN: 18kW@4.5K cold box (cds.cern.ch)



- ► HELIOS is composed of two main parts:
 - 1 supercritical helium loop
 - 1 saturated helium bath
- ▶ 2 heat exchangers ⇒ thermal coupling bath/loop
- ▶ Bath connected to the refrigerator (by HP & BP)
 - Cooling power available: 320 W
- ▶ Why Helios is used?
 - Supercritical helium loop is already available
 - Cold centrifugal pump ⇒ imposes forced convection
 - Saturated helium bath

 Interface with refrigerator +
 Thermal buffer

The test section

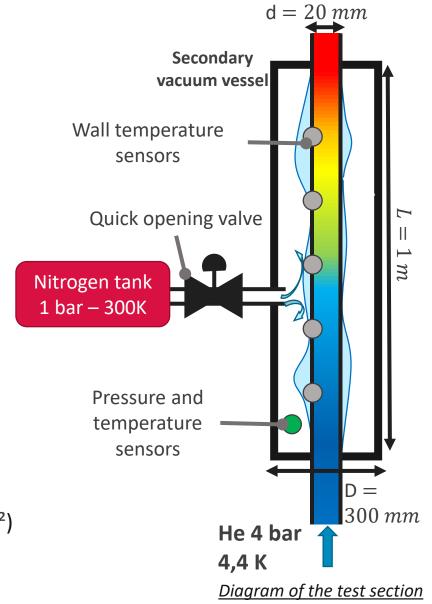
How to generate a « controlled » loss of insulating vacuum with HELIOS?

- ► A test section (TS) will be included in the helium loop of HELIOS
- ► Vacuum loss in a restricted area thanks to a secondary vacuum vessel
 - Vacuum break with N2 at atmospheric pressure/temperature
- ► Vertical upward supercritical helium flow

Hypothesis for the sizing of the experiment:

- $h_{condensation} \gg h_{forced\ convection}$
- Wall temperature imposed to 77K
- Supercritical He flow: 20g/s
- Dittus Boelter correlation

⇒ Heat load received by supercritical He ~ 2,7kW (4,25W/cm²)



Sizing of the new HELIOS loop

HELIOS has to be adapted to this new experiment

- ► Orders of magnitudes :
 - Estimated power transmitted to supercritical He in the test section: 2700W
 - Cooling power available: 320W

$$P_{section} \gg P_{refrigerator}$$

⇒ Thermal buffer need to be sufficient to store the energy injected during the loss of vacuum

- ► Last version of HELIOS:
 - Volume of the loop: ~30L
 - Volume of the bath: 310L

⇒ Not enough to keep the maximal pressure under the safety valve opening pressure (Pmax = 9 bar)

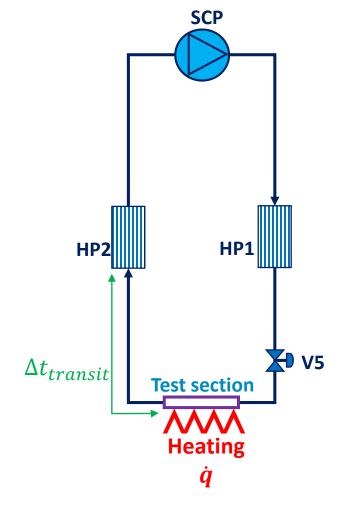
- Sizing parameters :
 - Volume of the loop
 - Transit time between the test section and heat exchanger
 - Thermal exchange loop/bath
 - Volume of the bath (thermal buffer)

Geometry of the loop

► The pressure increases due to the stored energy

$$egin{aligned} U_f &= U_i + rac{\dot{q} * \Delta t_{transit}}{m_{loop}} \ \Delta t_{transit} &= rac{
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ightarrow HP2}}{\dot{m}} \end{aligned}$$

- ▶ Volume distribution
 - Remove volume between TS and HP2 to reduced $\Delta t_{transit}$
 - Cold volumes to be added: HP2 SCP and HP1 TS

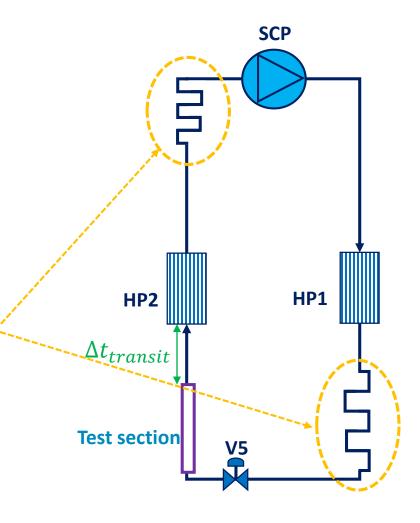


Geometry of the loop

► The pressure increases due to the stored energy

$$U_{f} = U_{i} + \frac{\dot{q} * \Delta t_{transit}}{m_{loop}}$$
$$\Delta t_{transit} = \frac{\rho V_{TS \to HP2}}{\dot{m}}$$

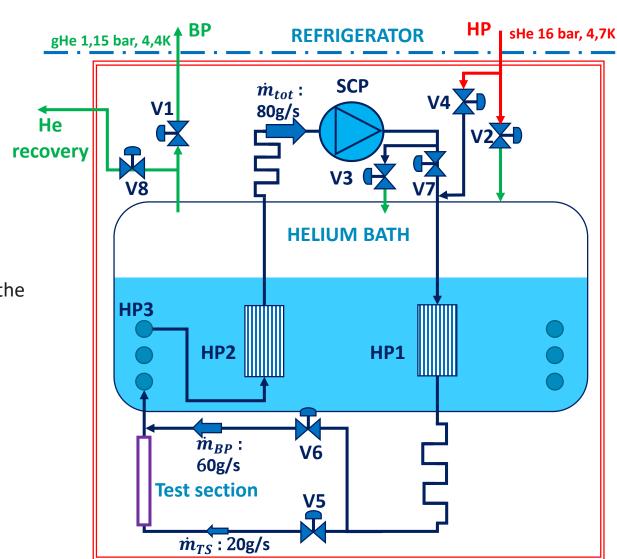
- ▶ Volume distribution
 - Remove volume between TS and HP2 to reduced $\Delta t_{transit}$
 - Cold volumes to be added: HP2 SCP and HP1 TS
- ▶ In the new loop design, the volume reaches 170L





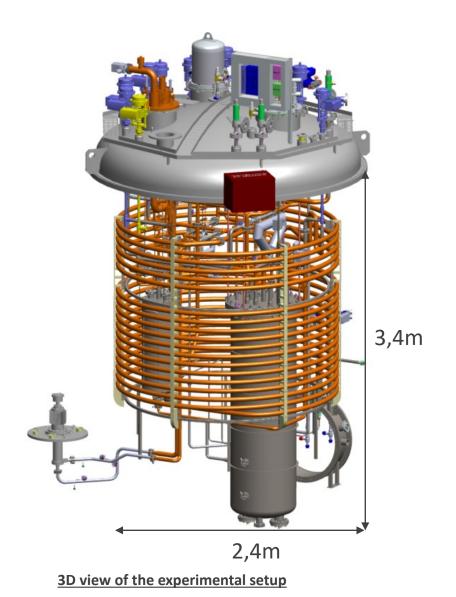
Additional modifications to the HELIOS loop

- ► A new heat exchanger has been added (HP3) :
 - Power injected in the TS >> Heat load used for the sizing of HP2
 - The new heat exchanger is placed between TS and HP2
 - 3 parallel copper coils immersed in the bath
- ► The by-pass line :
 - Large part of the flow by-passes the TS
 - Improves the additional heat exchanger (HP3) performances
 - The cold circulator can be used on an extended operation field
- ▶ The bath has been connected to the helium recovery system
 - Cold He gas can be evacuated from bath without passing through the refrigerator
- ▶ The bath volume was increased from 310L to 510L :
 - Space to include the new heat exchanger
 - Increased thermal storage





Some illustrations



Photography of the 3 heat exchangers



Photography of the bath

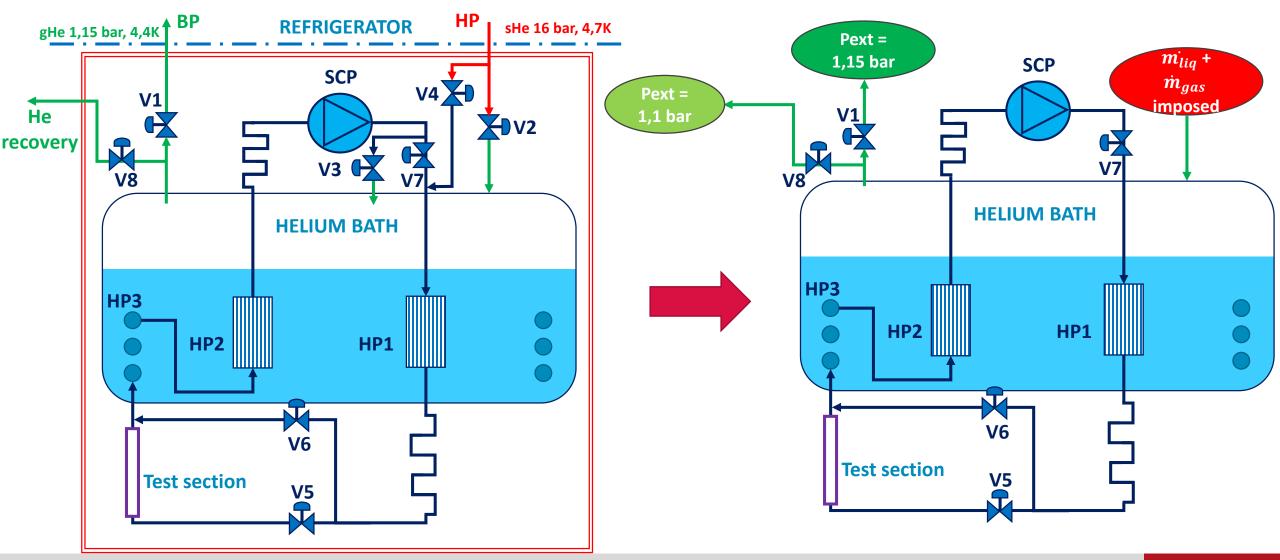
The CATHARE code



- ► Code for Analysis of Thermal Hydraulics during Accident and for Reactor safety Evaluation
- ► CATHARE: Reference tool for safety evaluation of pressurized water reactor, developed by CEA, FRAMATOME, EDF and IRSN since 1979
- ▶ Devoted to thermal hydraulic simulation of multiphase flow transient at the system scale
- ▶ 2-fluids and 6 equations model :
 - 3 equations for each phase: mass, momentum and energy balance
 - 6 main hydraulic variables: P, Hl, Hg, a, Vl, Vg
 - Taking into account all the flow regimes, mass and heat transfer between each phase or fluid and structure (~200 closure laws)
- ▶ The default fluid is two-phase water but other options are available:
 - Thermodynamic and transport properties of more than 100 fluids are available including helium (REFPROP database developed by the NIST)

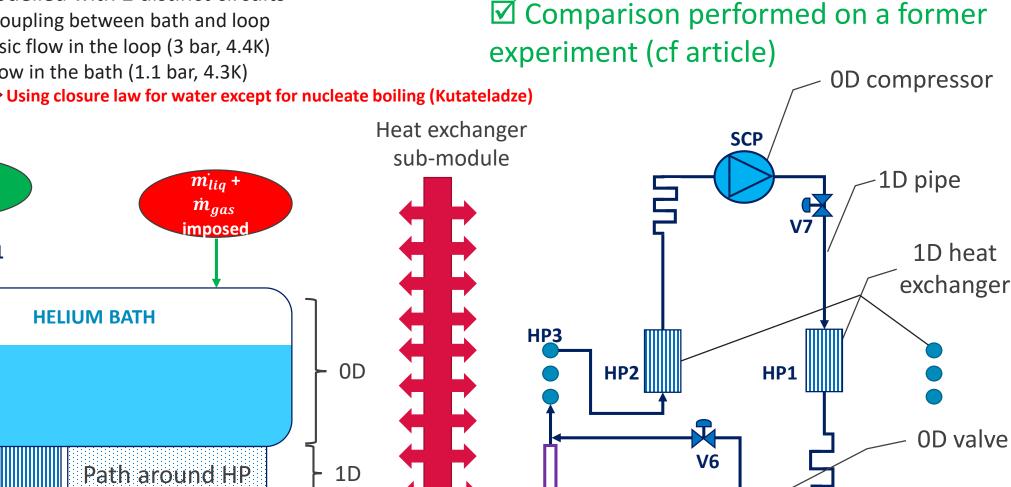


▶ Some simplifications are made on the modelling, using relevant boundary conditions



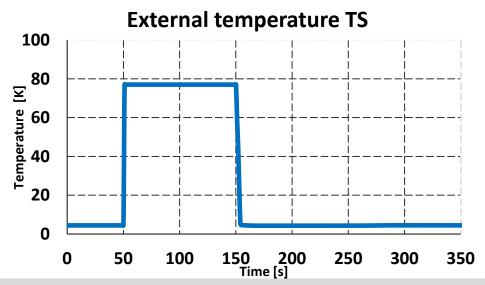


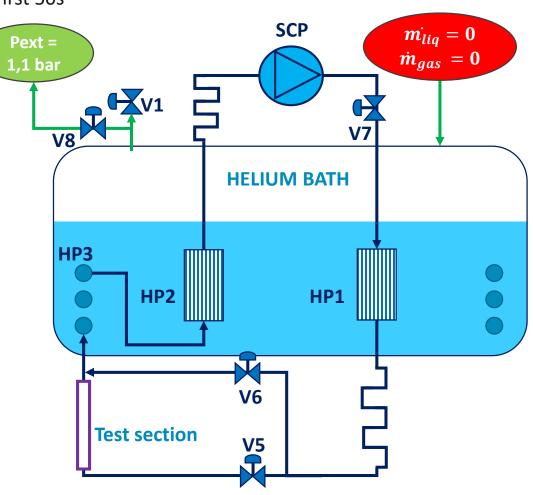
- ► The loop is modelled with 2 distinct circuits
 - Thermal coupling between bath and loop
 - Monophasic flow in the loop (3 bar, 4.4K)
 - 2 phase flow in the bath (1.1 bar, 4.3K)

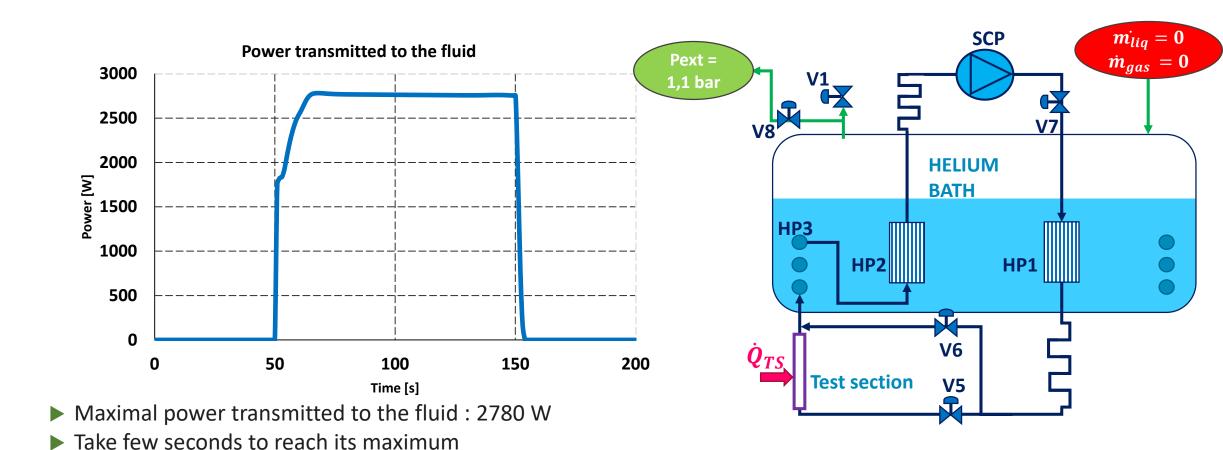




- ► Transient scenario :
 - Regulation only - $\Delta P_{SCP} = 0.85 \ bar$ (regulation on V7) / $\dot{m}_{SCP} = 75 \ g/s$ during the first 50s
 - $\dot{m}_{TS} = 20g/s$ (regulation on V5)
 - At t=50s : loss of vacuum
- ▶ Loss of vacuum : TS's external wall temperature imposed to 77K
- ▶ Bath isolated from the refrigerator, discharge in the He recovery
 - V1 close
 - V8 fully open

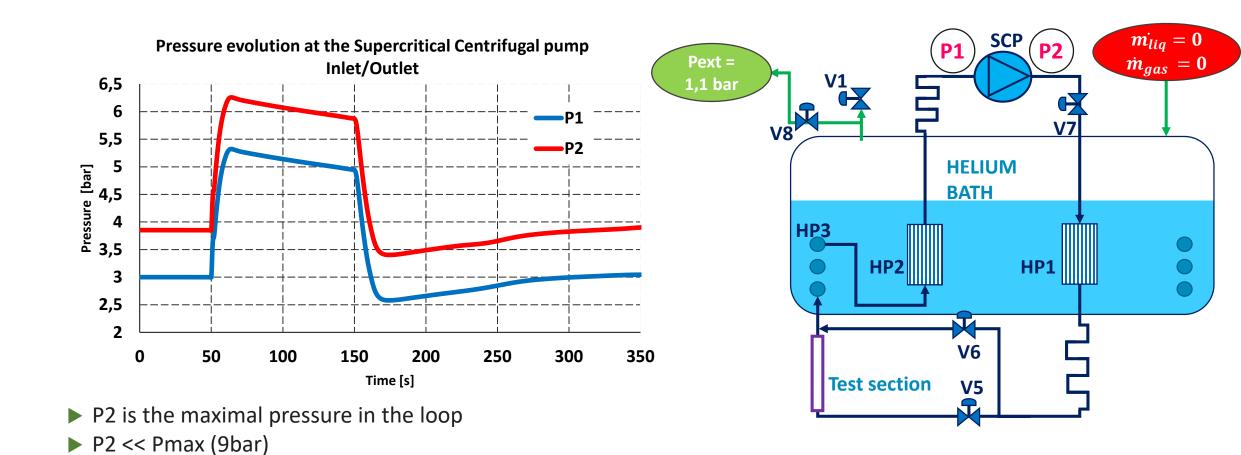




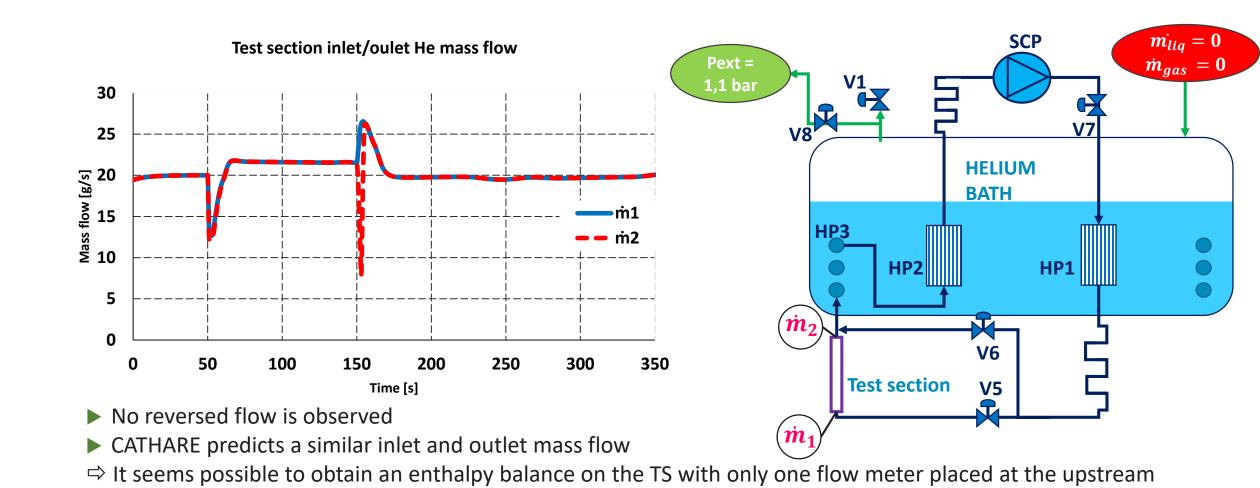


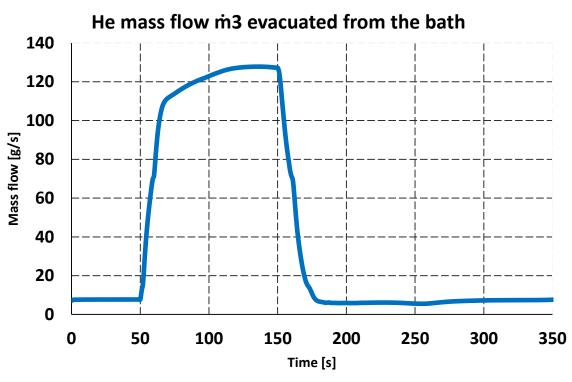
Mass flow decreases in the section due to the expansion of the heated helium

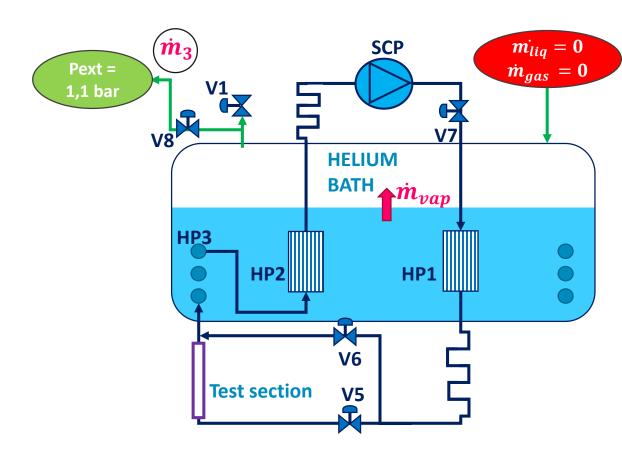




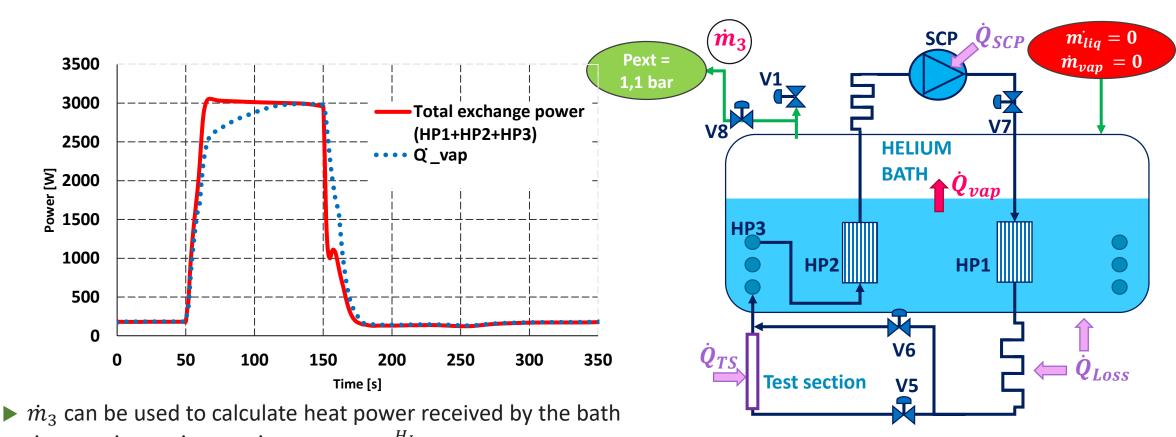
of the section







- ► For a <u>saturated bath</u> with <u>constant pressure</u>:
 - \dot{m}_{vap} is proportionnal to the power received by the bath
- ightharpoonup Only \dot{m}_3 can be measured : $\dot{m}_{vap} = \dot{m}_3/(1-\frac{\rho_v}{\rho_I})$
- ▶ Due to pressure loss (V8), the flow to reach its nominal value after a delay (P_{bath} increases from 1,1 to 1,17 bar)



 $\dot{Q}_{vap} = \dot{Q}_{TS} + \dot{Q}_{SCP} + \dot{Q}_{Loss} = \dot{m}_3 \cdot \frac{H_L}{1 - \frac{\rho_v}{\Omega_c}} = \dot{m}_{vap} \cdot H_L$

▶ To know the heat flux transmitted at the test section, all additional energy sources must be quantified

Conclusion



- ▶ A new design has been defined for the experimental device called HELIOS, in order to perform loss of vacuum on a dedicated test section and carry out experimental measures of heat flux
- ► CATHARE has been used to modelled HELIOS with its new design
 - The thermal hydraulic behaviour of the loop has been investigated
 - Sizing criteria is respected with the new design
 - Experimental methods to establish the heat flux transmitted the fluid with sufficiently low incertitude has been investigated
- ▶ The experimental set up is under construction :
 - Bath and the new heat exchanger are in place
 - Construction of the loop is expected to begin in October
- ► First experimental campaign expected in 2022
- ► Experimental result will be compared with CATHARE



Thank you for your attention