



Development of a multi-physic platform OLYMPE for fusion magnets design: progresses update and applications

DE LA RECHERCHE À L'INDUSTRIE

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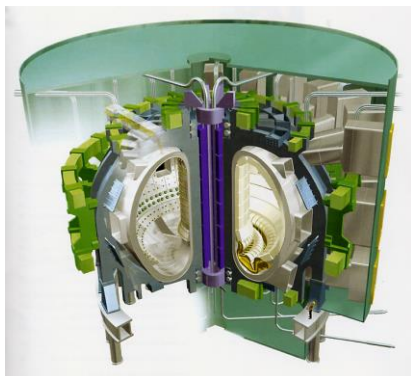
CHATS conference, 21st Sept. 2021

- **Introduction**
- **OLYMPE general presentation & status**
- **ElectroMagnetic-Design (EMD) bimodular loop**
- **ThermoHydraulic-Design (THD) bimodular loop**
- **ThermoHydraulic-Cryogenic-Design (THDC) trimodular loop**
- **Mechanical-Design (MECD) bimodular loop**
- **Conclusion-perspectives**

Tokamak **superconducting magnet** system design

→ multi-scale approach → several stages of analyses detail

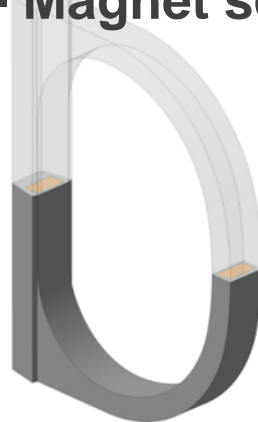
1- System scale



- Perimeter = reactor
- components (magnets, VV...)
- **macroscopic models** for components

↓
downscale

2- Magnet scale



- Perimeter = magnet envelope
- Major sub-elements (conductor, structures)
- **macroscopic models** for sub-elements (mechanics, EM...)

↓
downscale

3- Sub-magnet scale

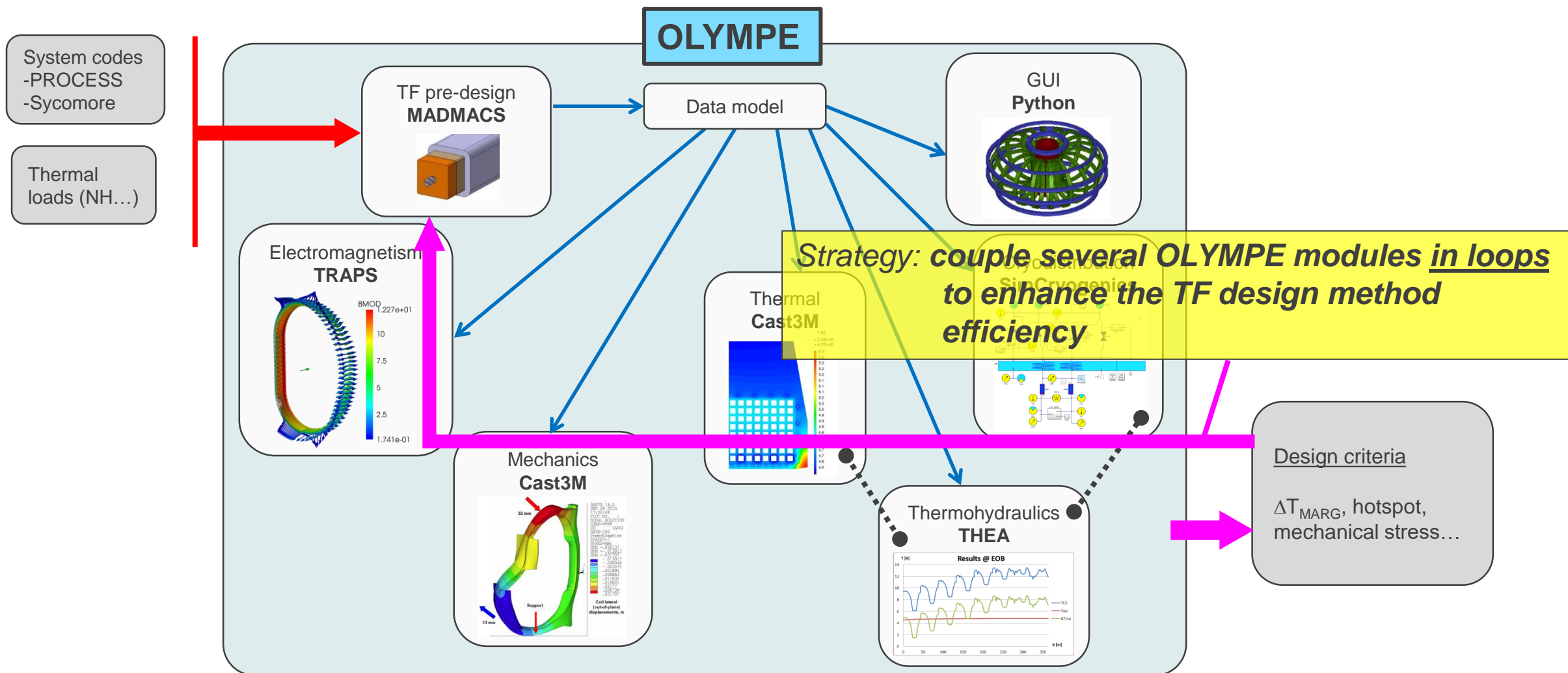


- Perimeter = subcomponent (conductor, insulation...)
- sub-elements details considered
- **Accurate models** of sub-elements (EM, thermohydraulic...),

complexity ↗ when scale ↘ : modelling & interfacing systems, calculation ressources...

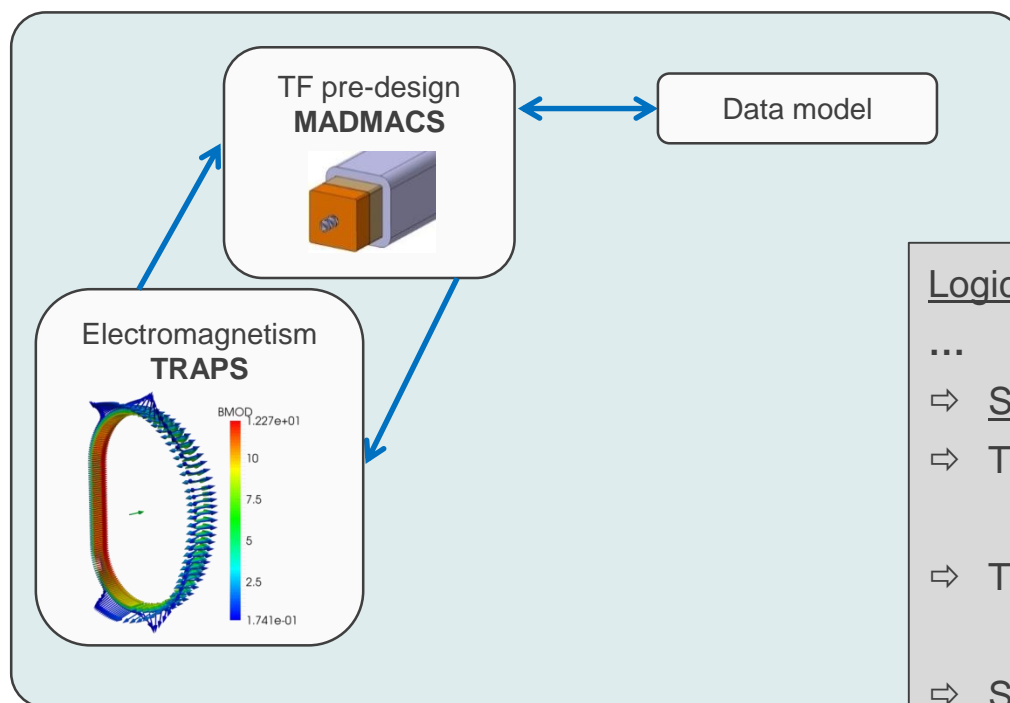
CEA develops an **integrated tool** which holds **variants in scales, physics & fidelity**

The platform is named **OLYMPE** (*plateforme multiPhysique pour aimants supraconducteurs*)



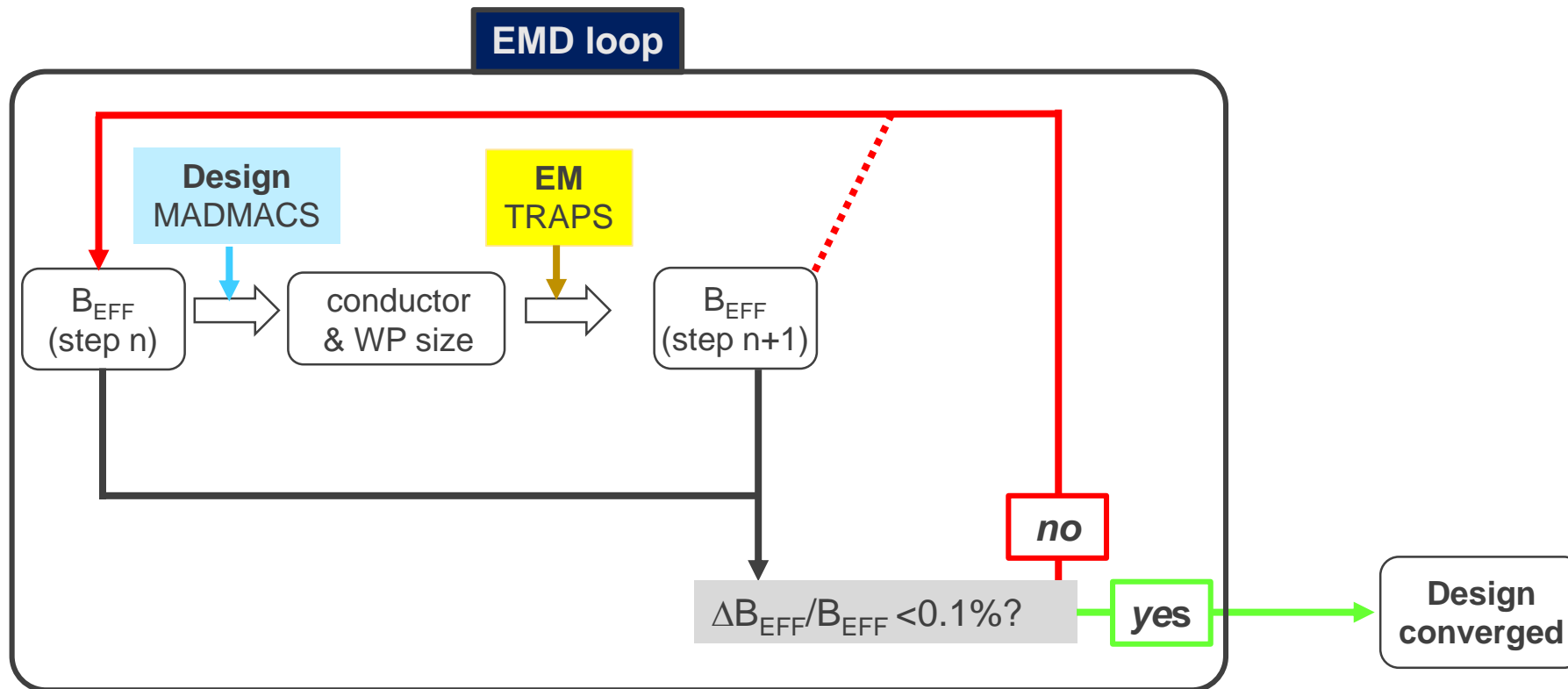
EMD purpose : issue a B_{EFF} -compliant TF design with regard to detailed analyses

ElectroMagnetic-Design loop



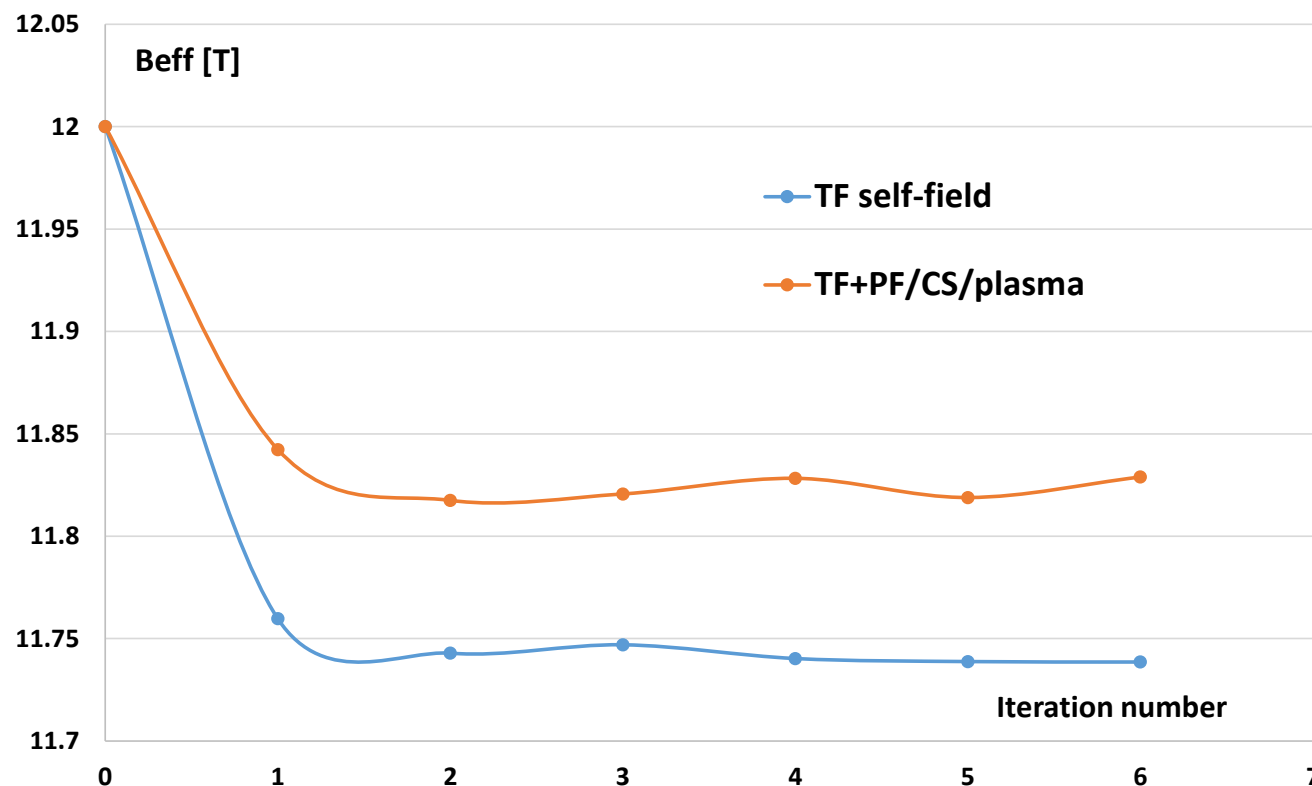
Logic flow

- ...
- ⇒ Step n : an effective field (B_{EFF}) is considered
- ⇒ The TF design is modified by this B_{EFF}
 - ⇒ **MADMACS** output
- ⇒ The TF design modifies B_{EFF} (current carriers topology)
 - ⇒ **TRAPS** output
- ⇒ Step n+1 : a new B_{EFF} is considered
- ...



- TRAPS time consuming (~10 min per run)
- Not fully automatized

An application is conducted on the **DEMO 2018 WP#3** configuration (pancakes winding, no radial plates)
TRAPS calculates the B map with 3D model (separated individual conductors, D-shape)



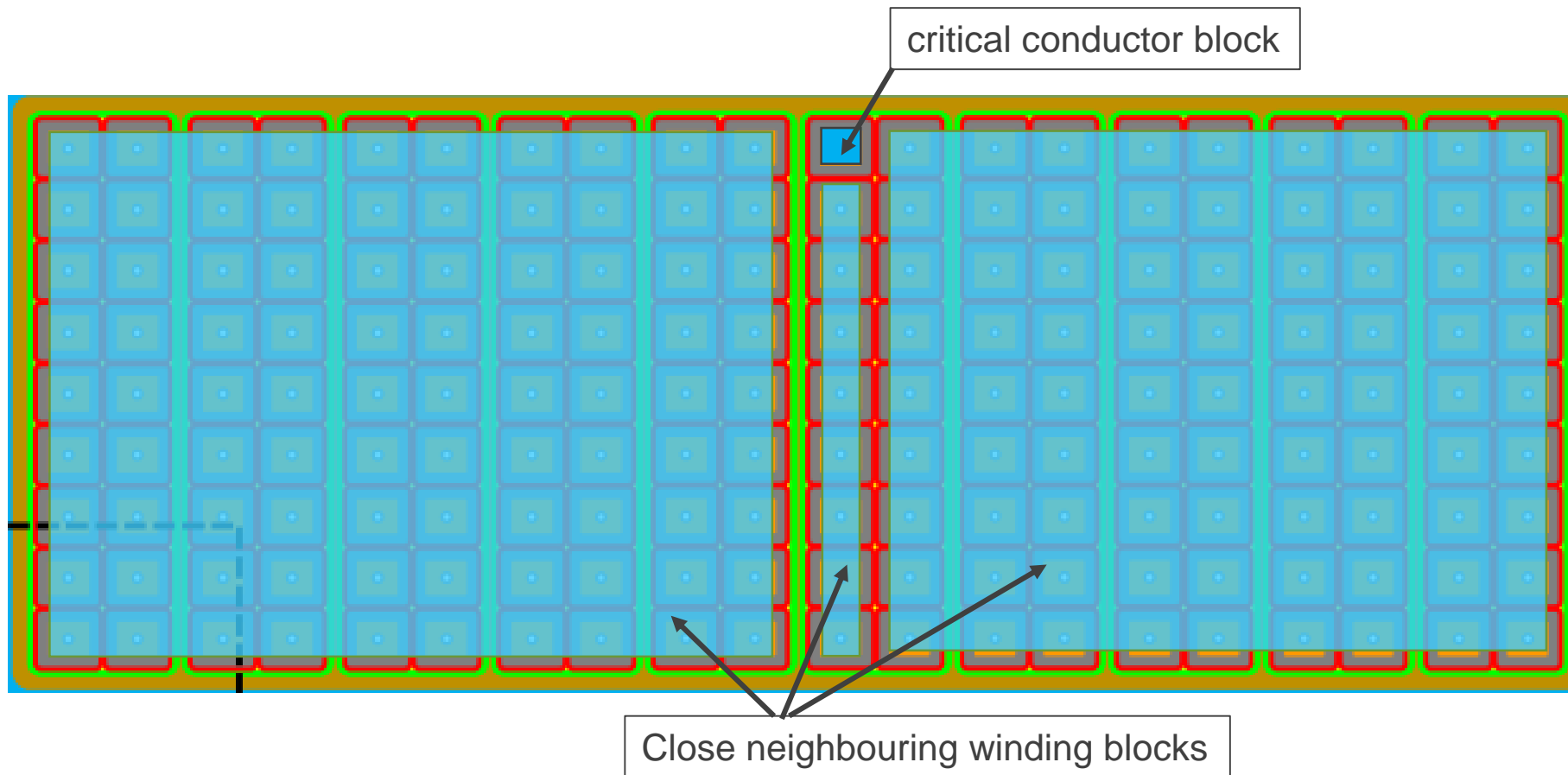
- Asymptotic behaviour after few iterations
- The TF self-induced configuration converges
- Independant B offset due to PF-CS creates small oscillations around close designs (1 strand difference)

- ➔ EMD loop is reliable and outputs self-consistent TF designs
- ➔ The computing time remains important
- ➔ Owing the fact that other loops should be aggregated (e.g. TH module) efficiency is addressed

B calculation efficiency is enhanced by considering a **full analytical approach**

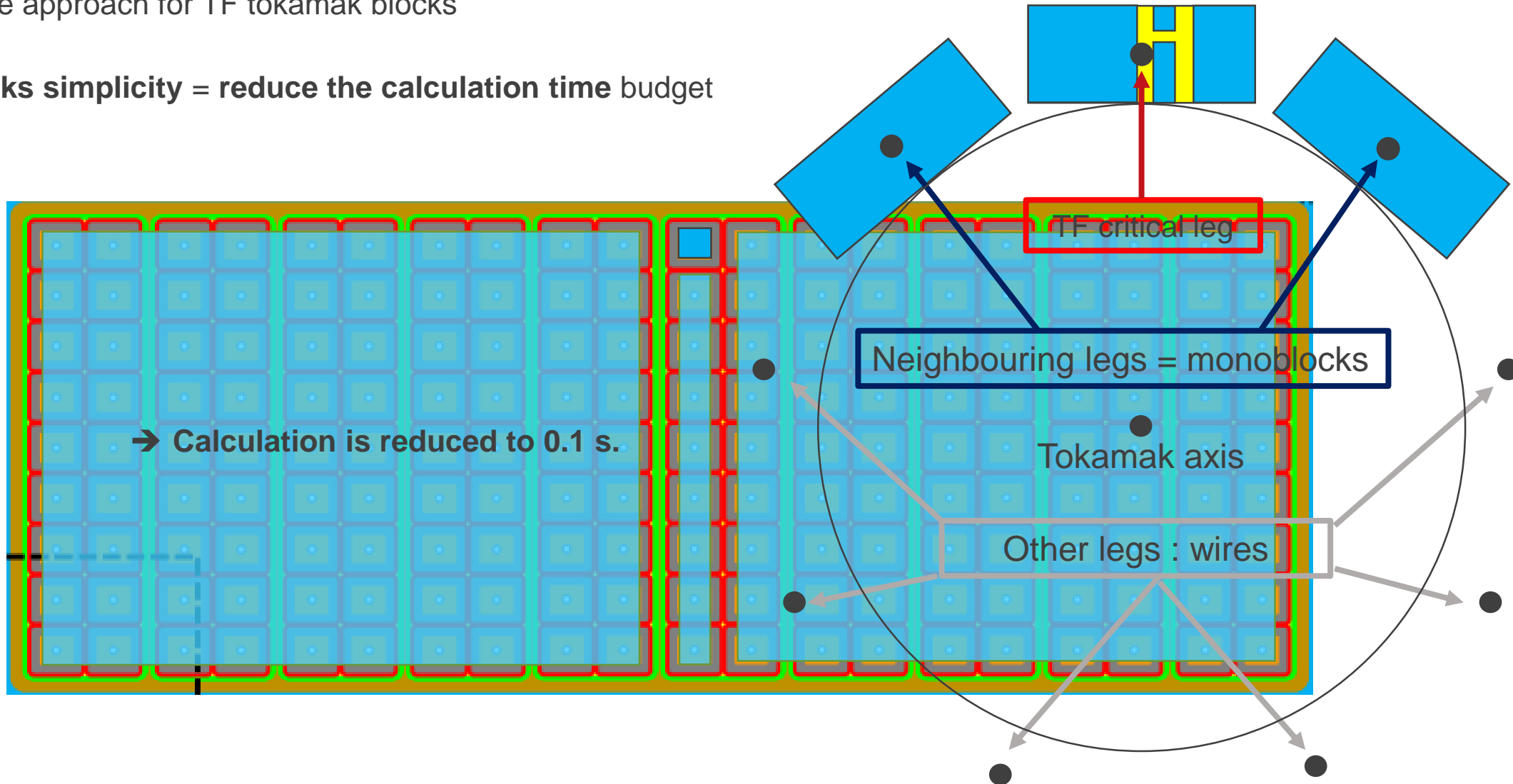
B map is set with **infinite current carrier** having rectangular section (analytical formalism)

B in critical zone is represented by **contribution of section blocks** which size depend on distance from critical zone

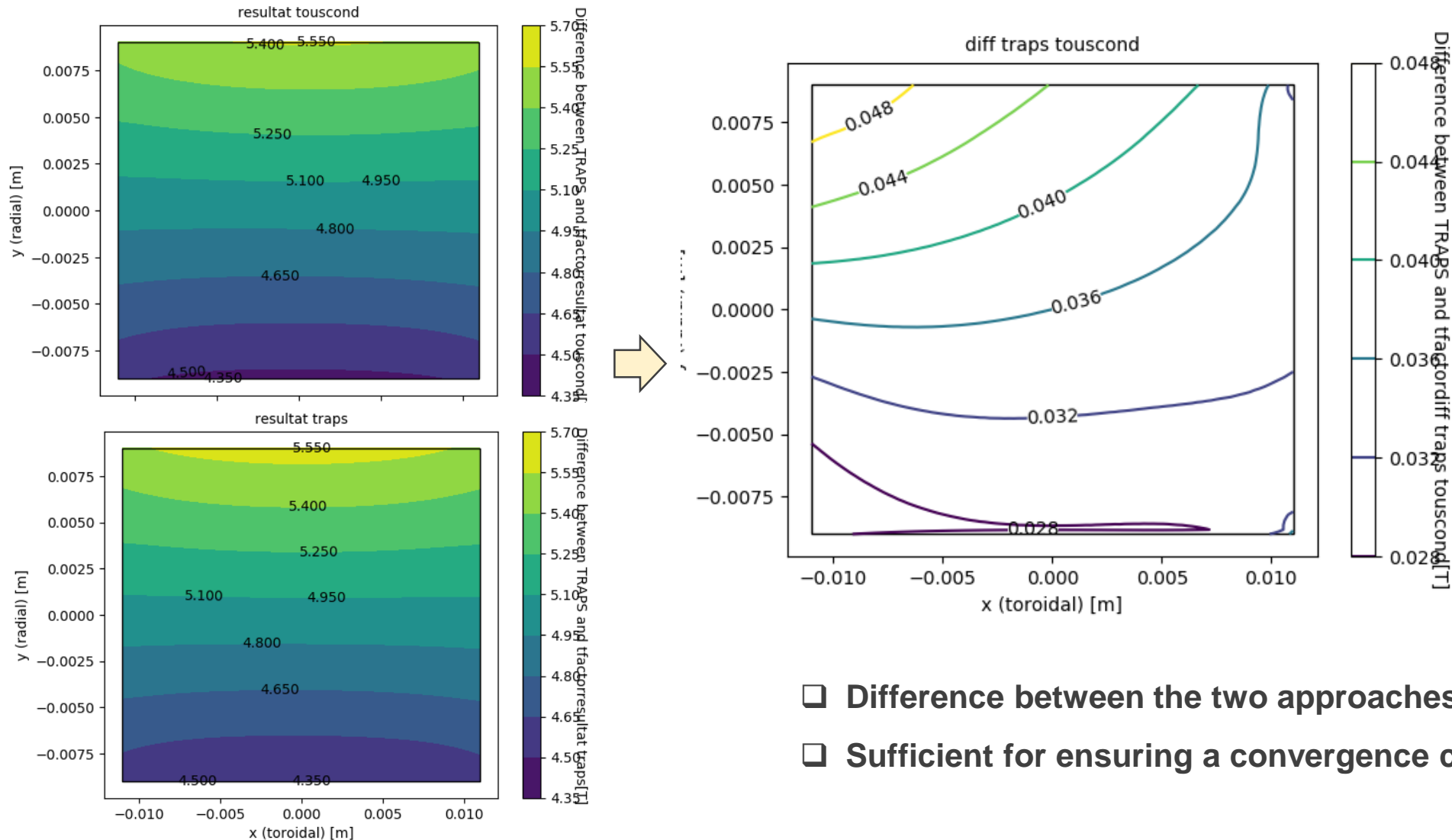


Same approach for TF tokamak blocks

Blocks simplicity = reduce the calculation time budget

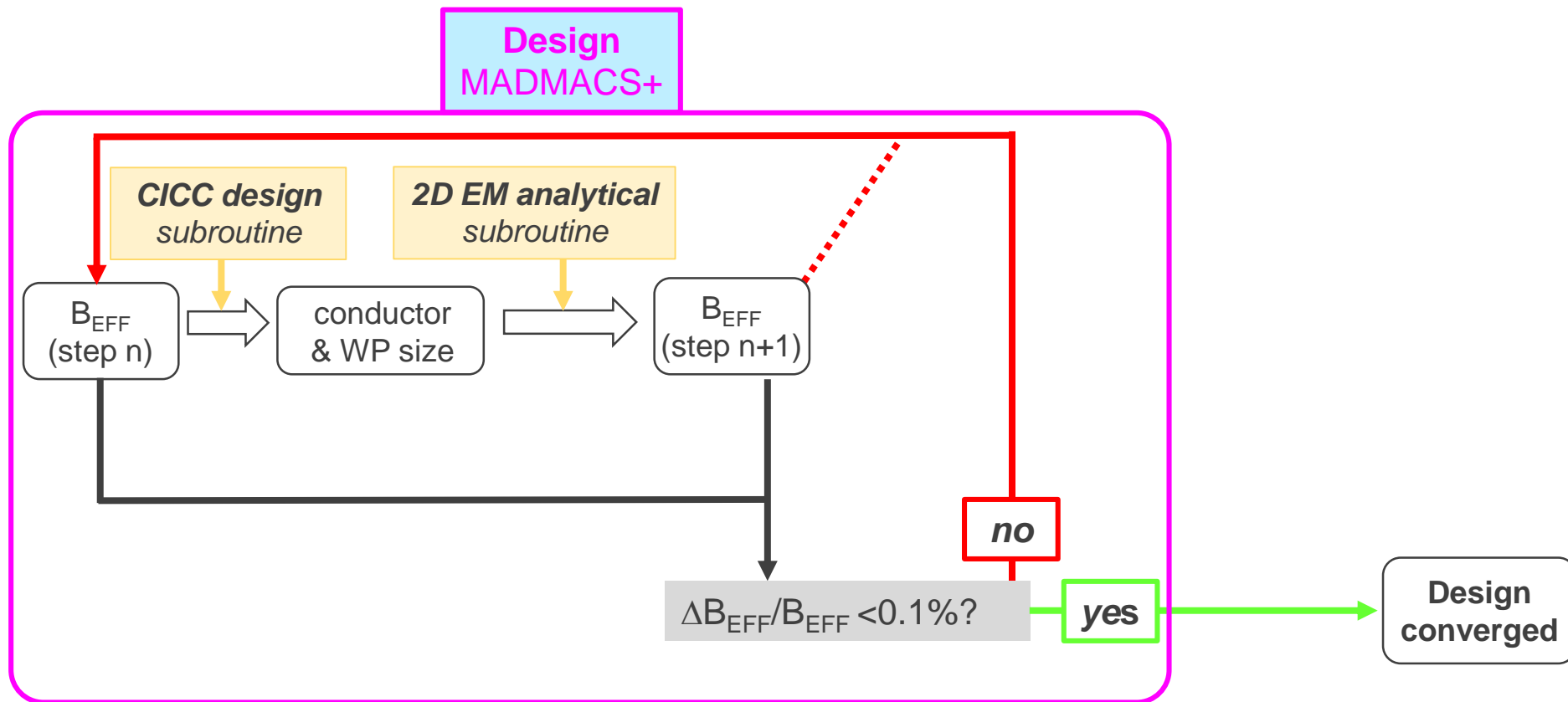


A benchmark of analytical approach (2D) with TRAPS (3D) was conducted on JT-60SA TF configuration



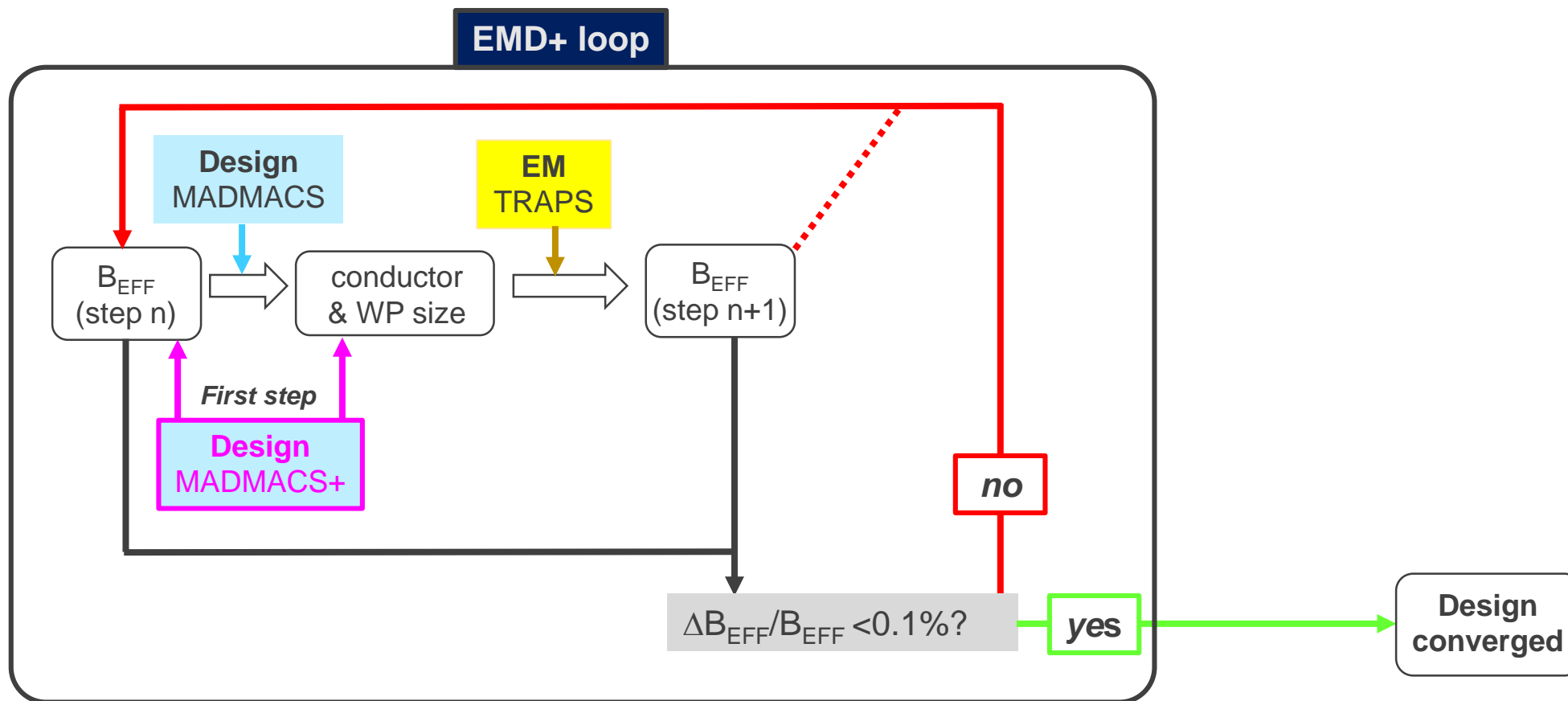
- ❑ Difference between the two approaches is $< 1\%$
- ❑ Sufficient for ensuring a convergence close to final state

The 2D EM analytical script was **integrated into MADMACS structure** (enhanced MADMACS+)



→ MADMACS+ calculation time < 1 second

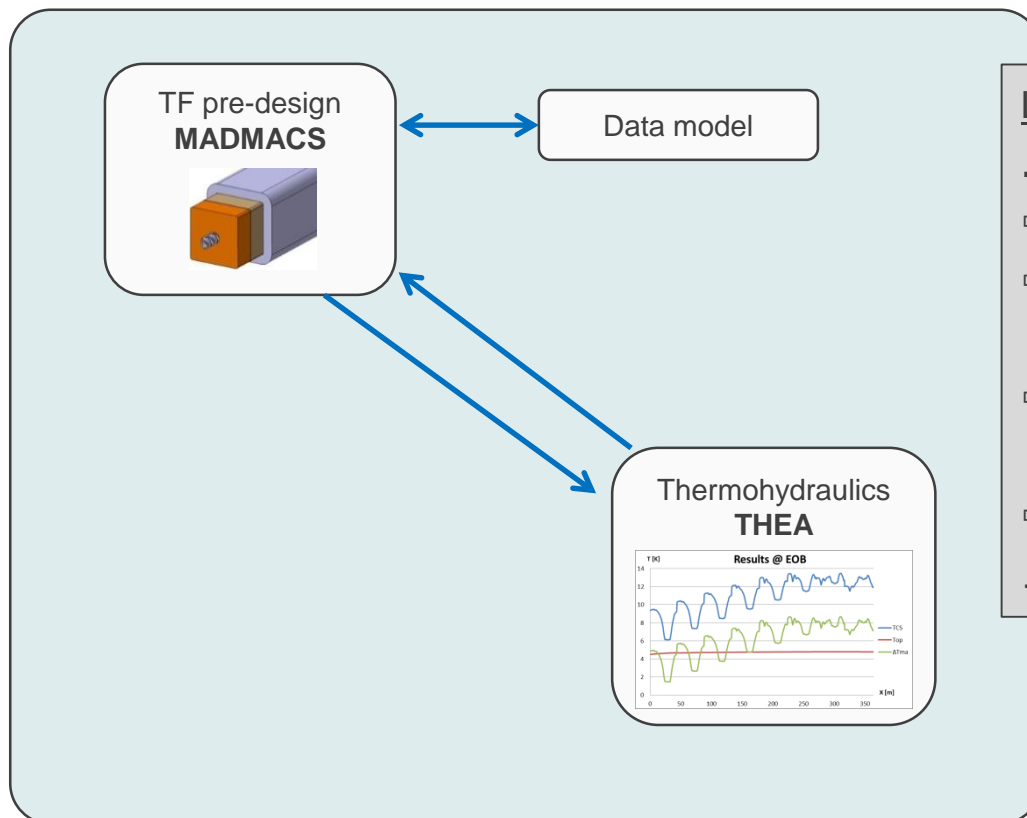
→ EDM+ loop: MADMACS+ convergence is placed before EMD loop (MADMACS & TRAPS)



- The EMD loop+ expected to run much less iterations with TRAPS (to be checked)
- EMD loop+ full automatization to be carried out

THD purpose: issue a ΔT_{MARG} -compliant TF design with regard to detailed analyses

Thermo-Hydraulic Design loop



Logic flow

...

⇒ Step n : an operation temperature (T_{OP}) is considered

⇒ a TF design is issued from this T_{OP}

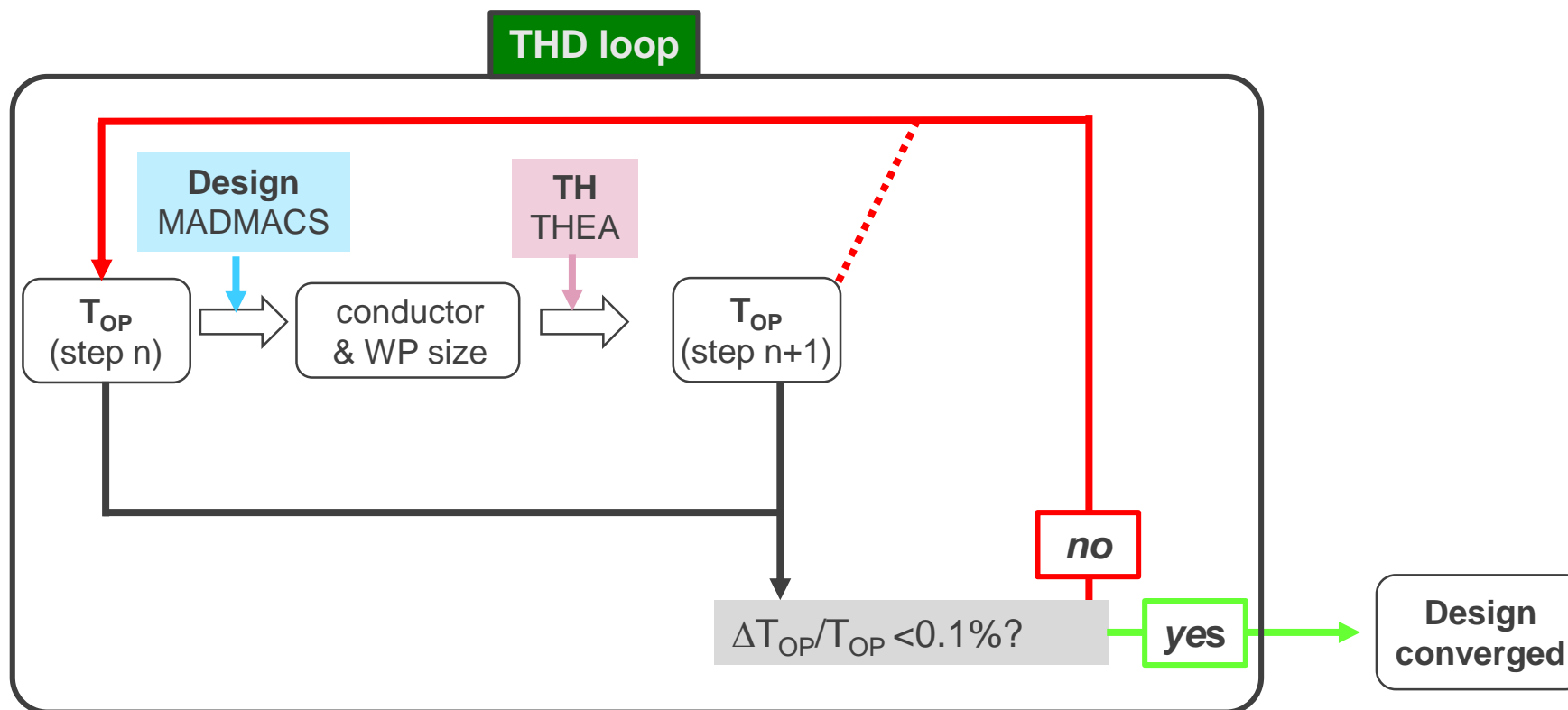
⇒ MADMACS output

⇒ The TF design modifies the T_{OP} (hydraulic properties)

⇒ TRAPS output

⇒ Step n+1 : a new T_{OP} is considered

...



- Fully automatized
- Run time is about 1 min per iteration \Rightarrow ~ 20 min usually for convergence
- EM considerations can be introduced with MADMACS+

MADMACS+ output is a single B_{EFF} value while THEA works with a 1D EM map $B(x)$

Initial $B(x)$ is with TRAPS for first step, for next steps $B(x)$ is shifted so that $\max(B(x))=B_{EFF}$

An **application** of the THD loop with MADMACS (original version) was initiated on DEMO 2018 TF WP#3 concept (pancake option without radial plates) : parametric exploration with different $[\Delta P, T_{IN}] \rightarrow$ ref [1]

Present objective :

conduct similar parametric studies but

- With more realistic thermal load on conductor (i.e. considering the load from structures)
- across a broader $[\Delta P, T_{IN}]$ range = $[0.5 - 1.5 \text{ bar}] * [2.5 - 4.5 \text{ K}]$
- MADMACS and MADMACS+ modules used to quote the effect of B_{EFF} variation with design across the spanned zone

A dedicated GUI was developped
(Python) for the THD loop



Inputs for THEA-MADMACS

Pressure drop in the conductor

Pin [bar] 15.0

DP [bar] 1.2

Values for inlet temperature

minimal Tin [K] 4.0

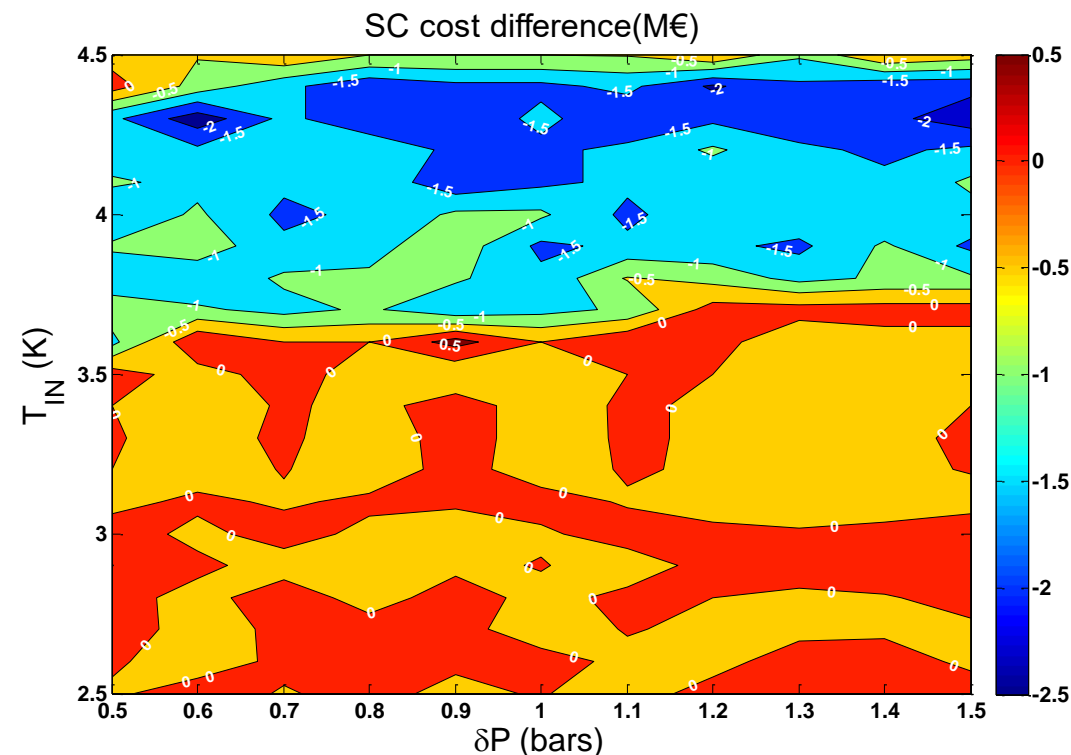
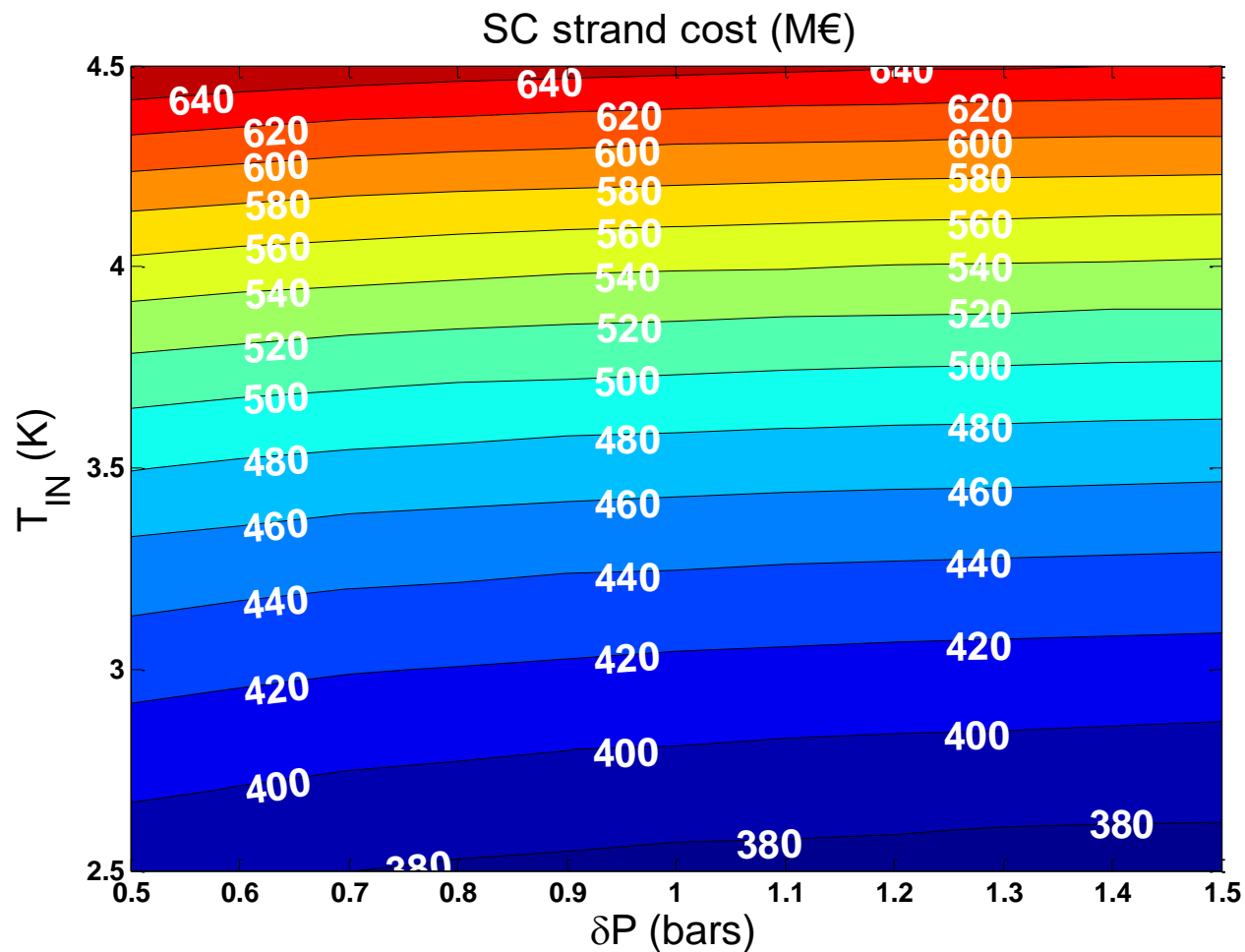
step increment Tin [K] 0.1

maximal Tin [K] 5.0

Compilation Execution

[1] Sandra Varin, François Bonne, Christine Hoa, Jean-Marc Poncet, Louis Zani, Benoît Lacroix, Quentin Le Coz, *Optimization of the overall Toroidal Field Coil cryomagnetic system at the pre-conceptual design phase of the European DEMO fusion reactor*, presented at SOFT 2020, to be published in Fusion Eng Design

As result both cases look similar



Differences are marginal as $\Delta \text{cost} < 1\%$

This derives from the small difference in conductor size and then in B_{EFF}

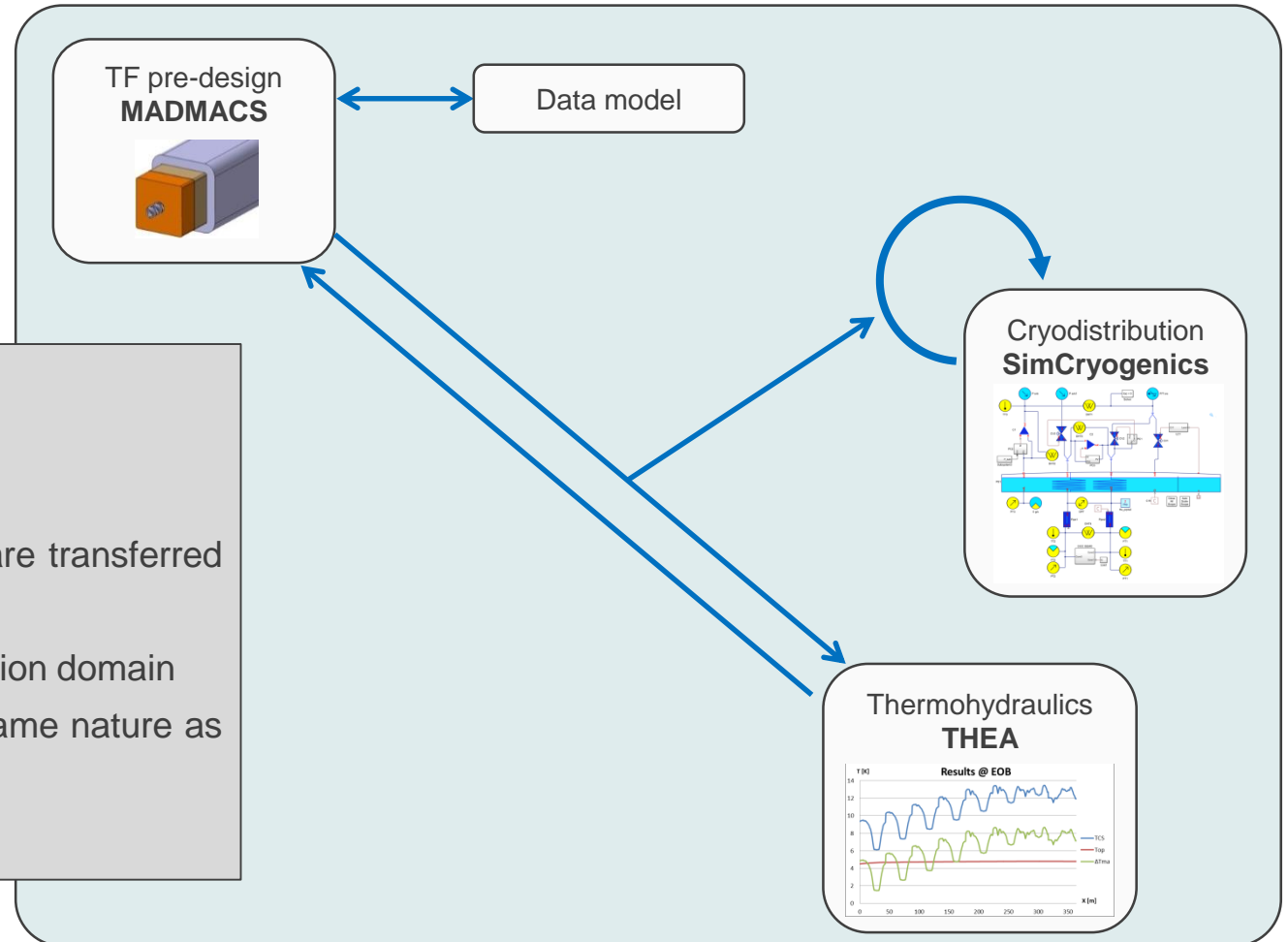
→ The B_{EFF} calculation functionality does not change much the global dependance with ΔP and T_{IN}

Objective: produce system-scale parametric studies considering magnet and cryoplant

Thermo-Hydraulic & Cryogenic Design loop

Logic flow

- ⇒ THD loop is run across an operation domain
- ⇒ THD loop outputs defined factors of merit
- ⇒ THD loop data useful for cryogenic design are transferred to Simcryogenics
- ⇒ Simcryogenics is run across the same operation domain
- ⇒ Simcryogenics outputs factors of merits of same nature as for THD
- ⇒ Factors of merits are combined



In the logic of extension to coupled cryo-magnetic TF system similar as in ref [1] we carried out a parametric exploration with different $[\Delta P, T_{IN}]$ with the same conditions as in THD loop example

The purpose is to combine the cost variations of the TF system and cryogenics systems across the $[\Delta P, T_{IN}]$ range.

As per **TF magnet part** we retained the outputs obtained with MADMACS+ module (see previous)

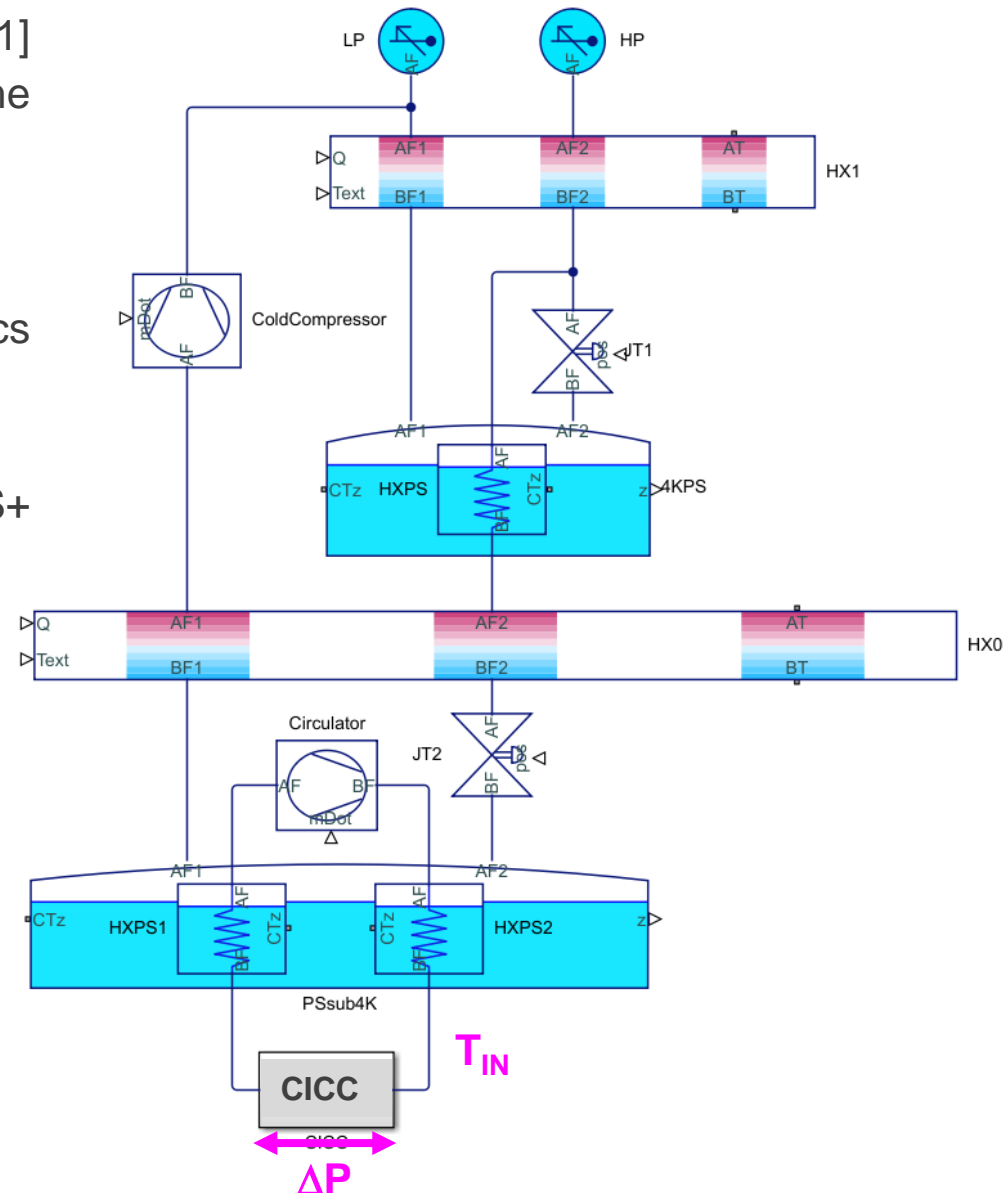
As per **TF cryogenic part** the configuration retained is a 2 bathes structured cold end with a 4.4 K bath that feeds a subcooler bath at $T_{in} - 0.2$ K .

→ The cost of the cryogenic part is divided in two :

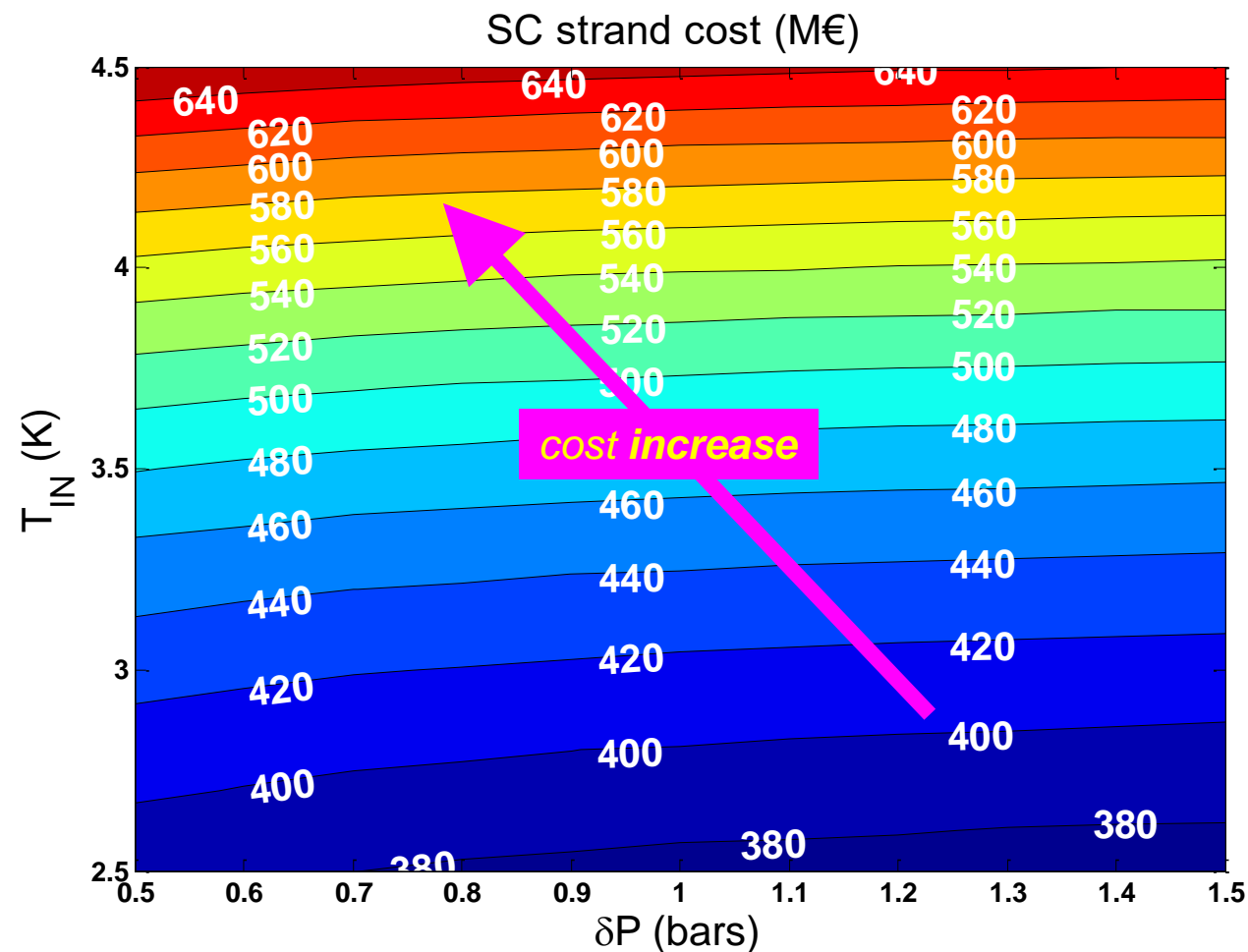
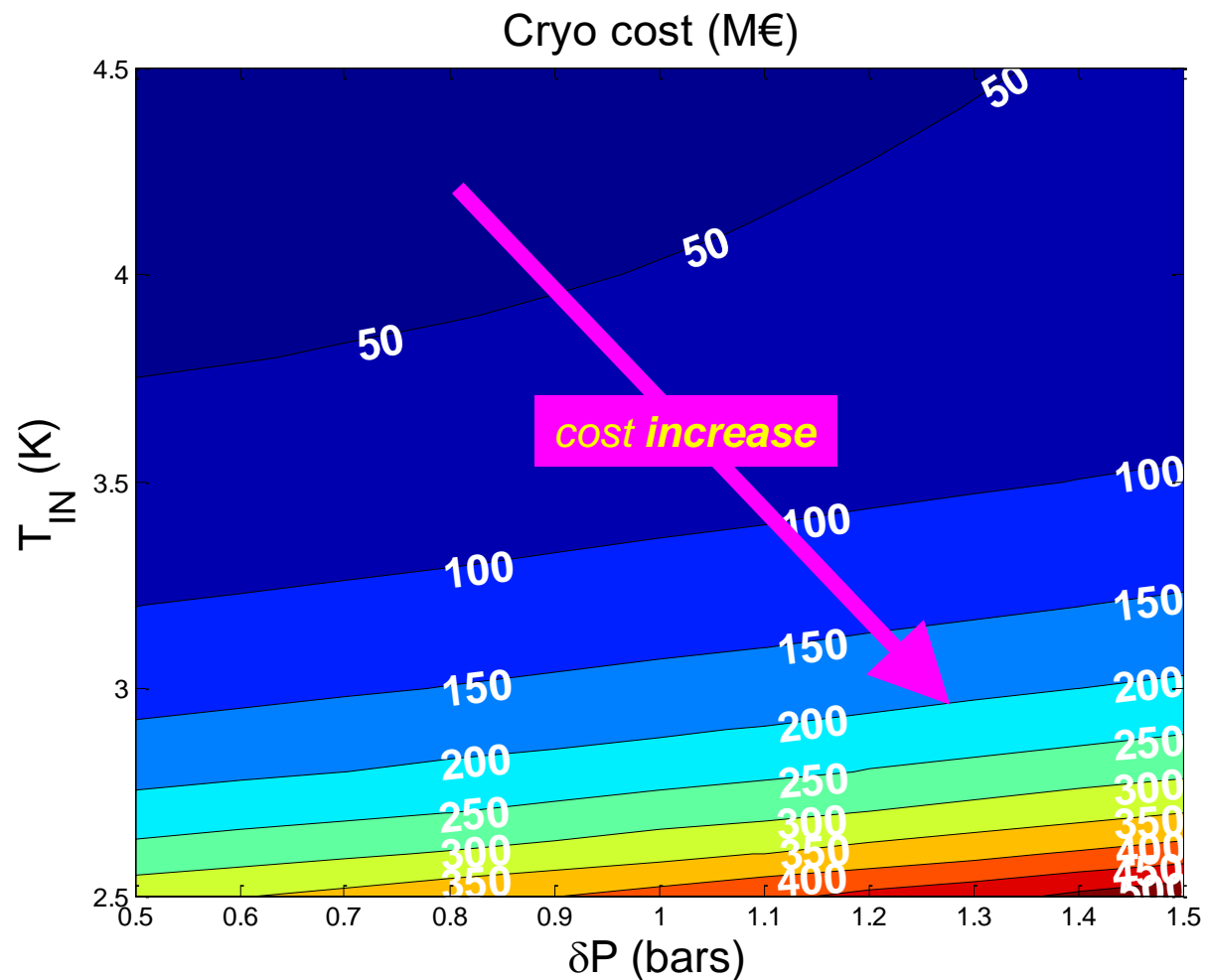
- Investment cost estimated with the Green formula

$$CAPEX = 2.9 \times P_{eq,4.5K}^{0.63} (kW)$$

- Operational cost is estimated with the electricity cost over 20 year exploitation



As result on the TF cryomagnetic system we obtain



Cost combination claims for an optimum...

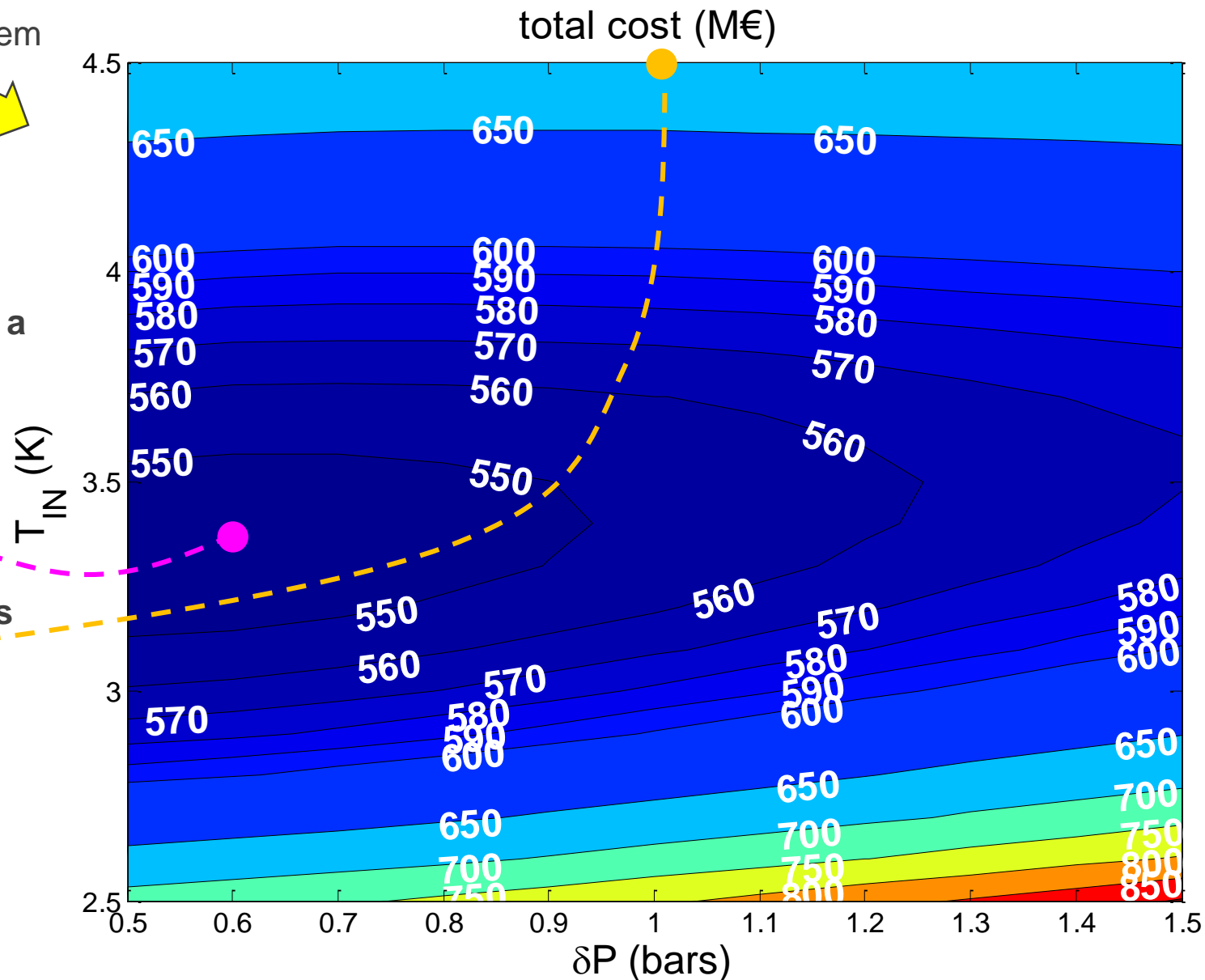
Result on the overall cryomagnetic TF system



→ The overall system cost spans across a broad range (545 ~ 900 M€)

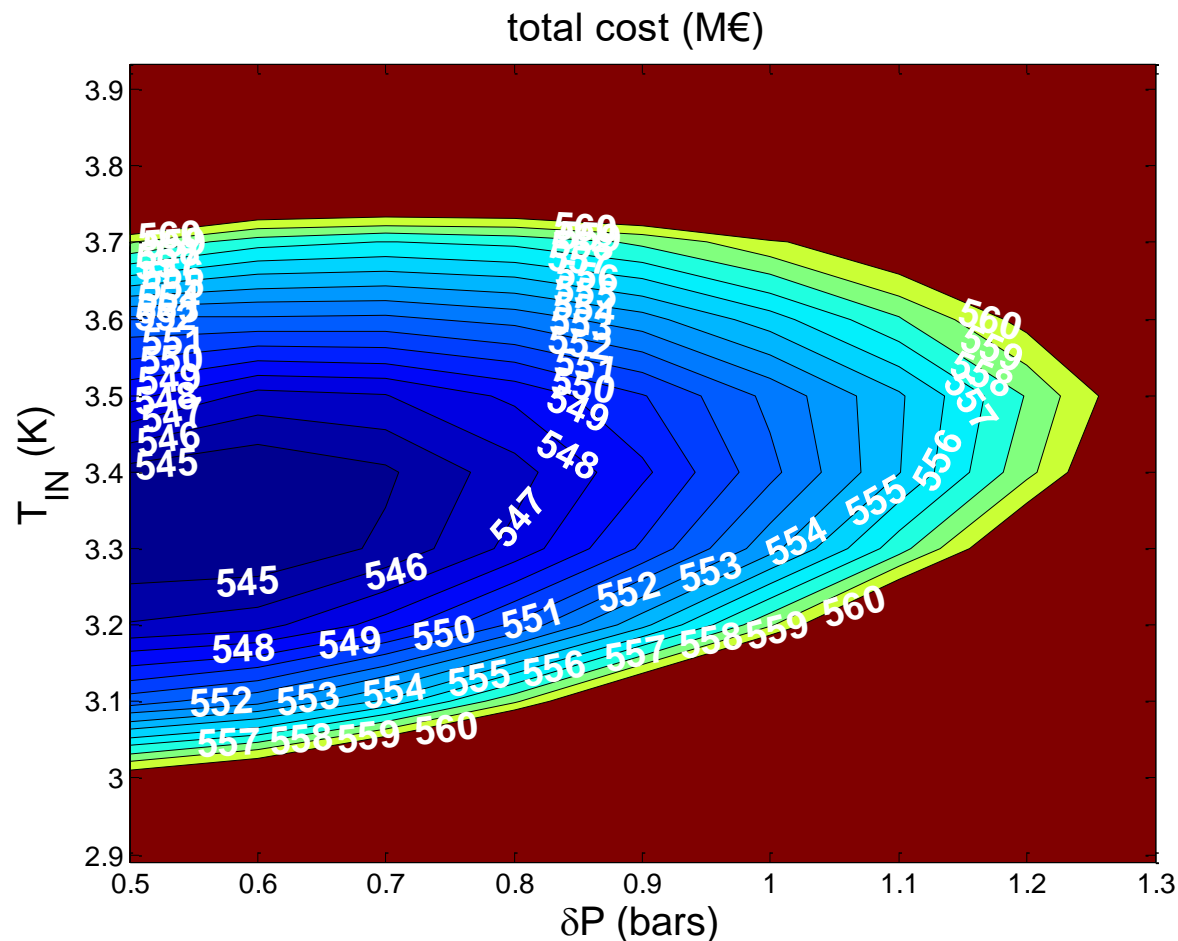
→ An absolute minimum is found at
~ $[T_{IN} = 3.4 \text{ K } \Delta P = 0.6 \text{ bar}]$
minimum cost is ~ 545 M€

→ Compared to DEMO nominal conditions
 $[T_{IN} = 4.5 \text{ K } \Delta P = 1 \text{ bar}]$
cost difference is ~ 140 M€



Discussion: is the minimum shallow or steep ?

A **3% decision flexibility margin** is considered to identify the boundaries of optimized operation domain



- ❑ On ΔP dimension, the minimum is rather shallow and any value of ΔP between 0.5 and 1.2 bar seem appropriate
- ❑ Conversely minimum is steeper across T_{IN} dimension, claiming for a T_{IN} between 3 K and 3.7 K

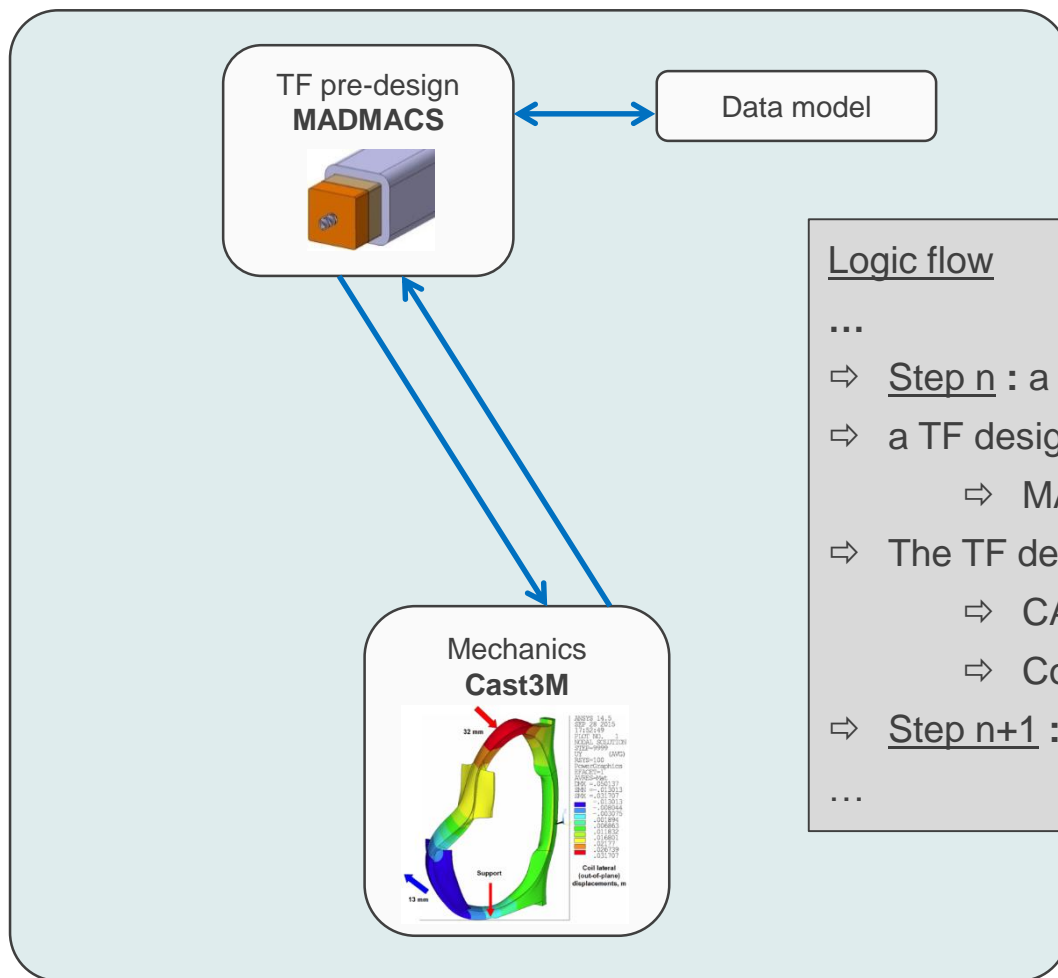
→ As per cost merits, the overall TF cryomagnetic system optimum pushes for low temperature operation

Perspectives

- Refine cost merit functions
- Consider technological choices (cryo...)
- Extend to the whole cryomagnet system (CS, PF)

MECanical **D**esign loop

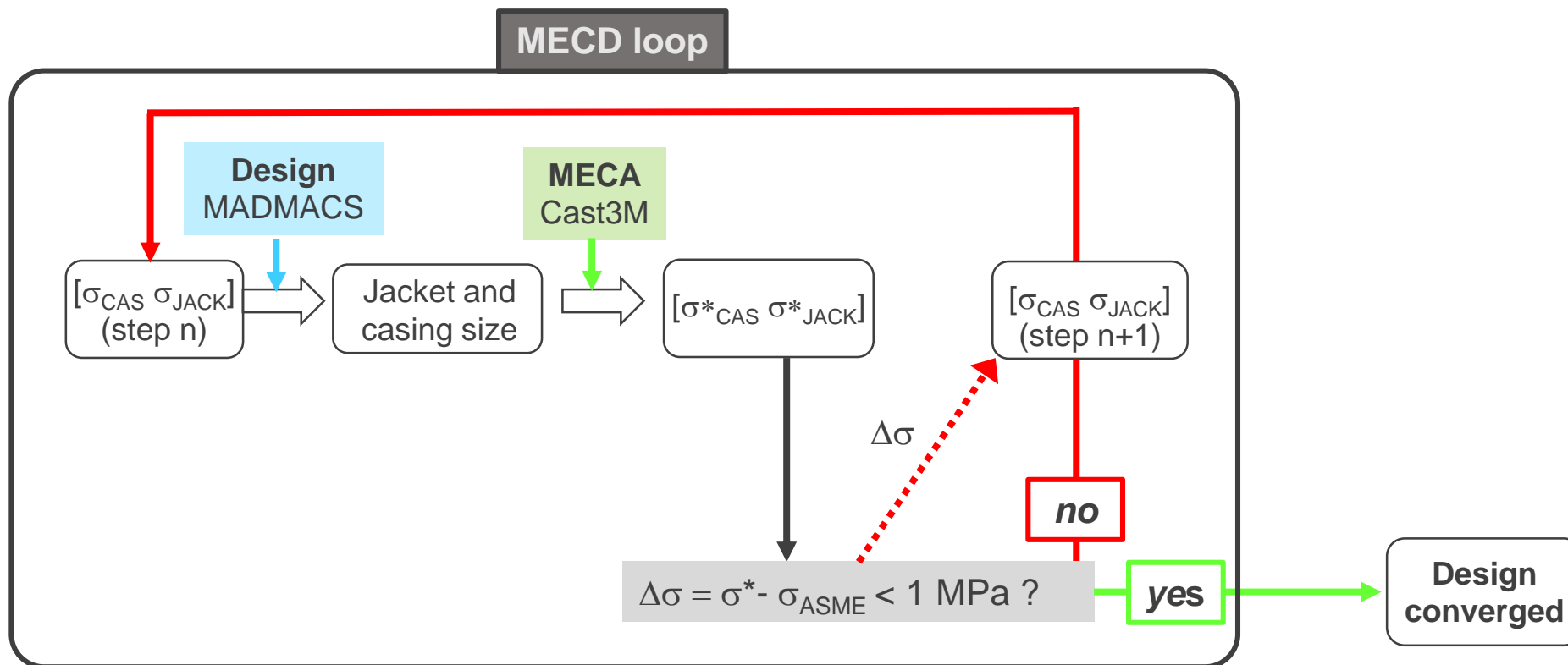
Objective: issue a stress-compliant TF design with regard to **detailed mechanical** analysis

Logic flow

...

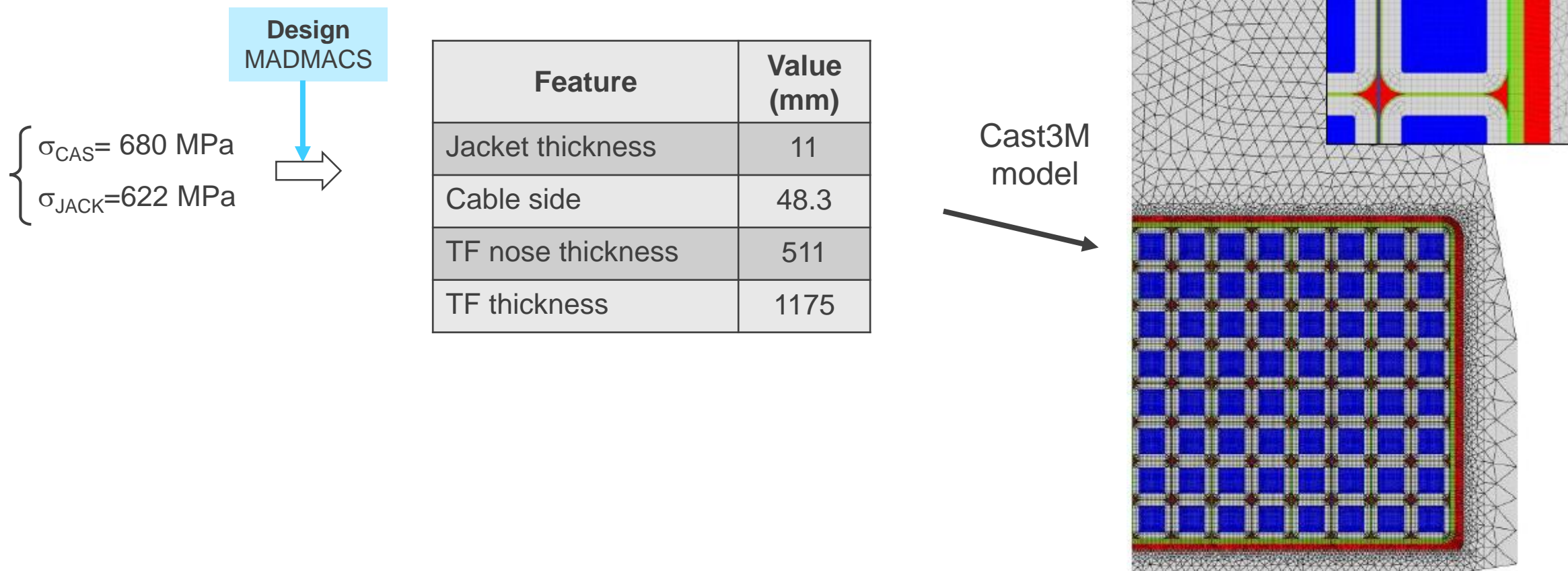
- ⇒ Step n : a couple of stress values (σ_{CASING} σ_{JACKET}) is considered
- ⇒ a TF design is issued from this (σ_c σ_j) (**macroscopic analysis**)
 - ⇒ MADMACS output
- ⇒ The TF design develops local (σ^*_c σ^*_j) (**detailed analysis**)
 - ⇒ CAsT3M output
 - ⇒ Comparison with ASME limits ($\Delta\sigma_c$ $\Delta\sigma_j$) **defined**
- ⇒ Step n+1 : a new (σ_c σ_j) is considered

...



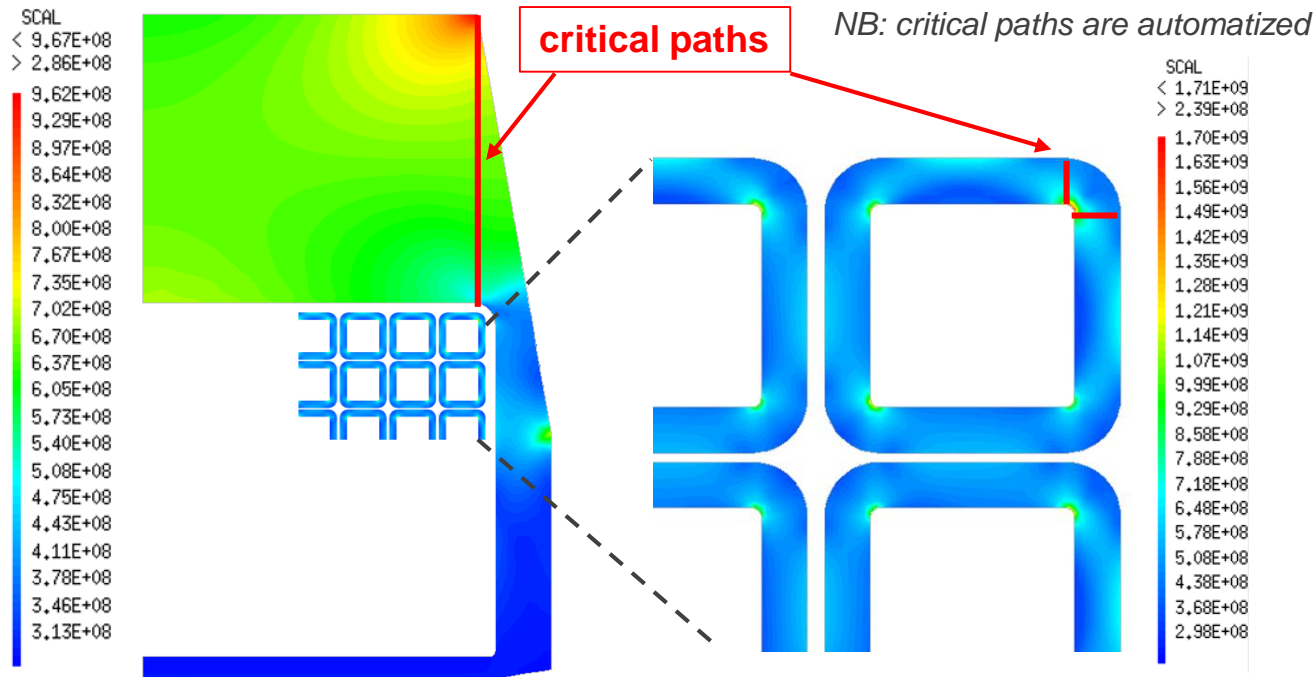
- Cast3M time consuming (~2 hours per run)
 - *can be improved (friction considered, GPS method not optimized...)*
- Data exchanges in loop not yet automatized

The first application attempt is conducted on **DEMO 2015 TF WP#3 concept**



NB: MADMACS Excel version is used for first attempt to ensure a stable optimisation with respect to both σ

Detailed analysis of DEMO 2015 load case



Casing stress map

Jacket stress map

Location	Membrane stress (MPa)	Margin to ASME (MPa)
Casing	616	+ 50
Jacket	568	+ 100

$$\left\{ \begin{array}{l} \sigma_{\text{CAS}} = 680 + 50 = 730 \text{ MPa} \\ \sigma_{\text{JACK}} = 622 + 100 = 722 \text{ MPa} \end{array} \right.$$

Design
MADMACS

Feature	Value (mm)	Δ (mm)
Jacket thickness	8.7	-2.3
Cable side	48.3	0%
TF nose thickness	480	-31
TF thickness	1100	-75

- Thinner jacket
- TF coil smaller radial buit

- new Cast3M run to be conducted
- MECD loop operability to be assessed
- Consider membrane + bending criterion

- In the framework of **OLYMPE** development **several multi-physic design loops** were built using the different modules of the platform
- **Electromagnetic Design loop** was established with a two-stages approach
 - ✓ An integration ni MADMACS was carried out for analytical part (moderate fidelity)
 - ✓ An hybrid loop is combined with TRAPS (high fidelity)
- **Thermo-hydraulic Design loop** was established
 - ✓ A parametric study [ΔP , T_{IN}] was conducted on DEMO configuration
 - ✓ In this application considering B_{EFF} variation with design has margina impact on results
- **Thermo-hydraulic Cryogenic Design loop** was established
 - ✓ The parametric study [ΔP , T_{IN}] was extended conducted on DEMO configuration
 - ✓ A global optimum for cryomagnetic system was found, claiming for low temperature operation
- **Mechanical Design loop** was established
 - ✓ A first try on DEMO 2015 was attempted to be consolidated



- Assess all loops convergence along their actual maturity (EMD, THCD, MECD...)
- Develop data exchange automatization and GUIs
- Run several application cases to establish their convergence stability
- Improve time computation budget
- Extend to all tokamak systems (CS, PF)



Thank you for your attention

Questions ?