

PRELIMINARY CONCEPTUAL DESIGN OF THE COMPASS UPGRADE ECRH HEATING SYSTEM

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COMPASS UPGRADE

COMPASS upgrade tokamak is currently under design and construction. First plasma end of 2025.

[Vondracek et al., Fusion Eng. Des. 2021]

Major radius: **0.9 m**

Minor radius: **0.27 m**

Toroidal magnetic field: up to **5 T**

Plasma current: **2 MA**

Flap top: **1-10 s** (3 s for 5T and 2 MA scenario)

Line average density: $\approx 2.8 \times 10^{20} \text{ m}^{-3}$

Central electron temperature: $\approx 4 \text{ keV}$ (up to **7 keV**)

Additional heating

NBI: 3 units with 2 ion sources => **3-6 MW**

ECRH: 2 equatorial ports for heating => **2-6 MW**

incline port for NTM suppression => **1 MW**

Scientific program

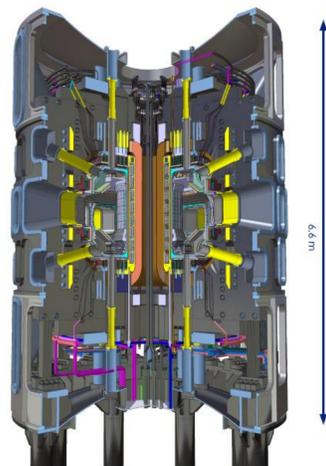
edge plasma physics and advance confinement mode research

NTM studies and suppression technique

Runway electrons generation and mitigation

Test of liquid metals divertor concepts

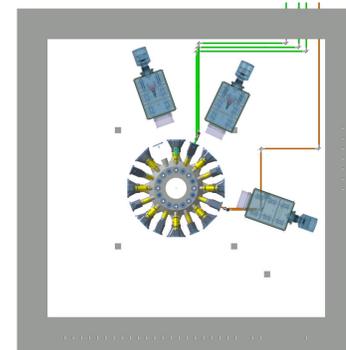
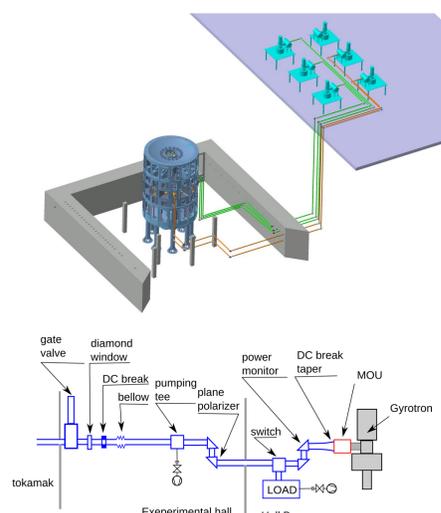
Hot first wall operation (up to 500 °C)



TRANSMISSION LINE

Sectors allocated for ECRH are the midplane narrow ports #16 and #12

Gyrotrons will be located on the third floor of the new building. Waveguides will enter the hall from the floor bellow and will reach the tokamak from below.



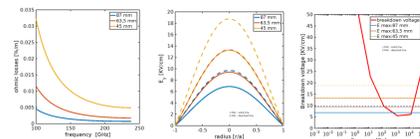
	length [m]	miter bend	losses [%]
Port # 16	40	8	~4,5
Port # 12	47	9	~4,8

Transmission line components placement

Waveguide:

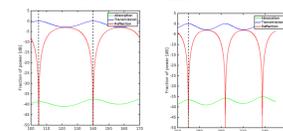
Evacuated corrugated waveguide: optimizes for the 140 GHz, period: 0.63 mm ($0,3 \cdot \lambda_{140}$), depth 0.52 mm, width 0.44 mm

material Aluminium and SS



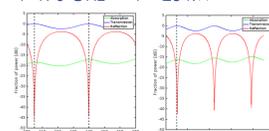
Losses, electrical field and breakdown voltage for different waveguide diameter and 140 GHz.

CVD diamond disc
d=1.8 mm/1.85 mm, $\tan \delta = 1 \times 10^{-5}$, $\epsilon = 5.67$
f=105 GHz => P= 130 W, f=140 GHz => P= 180 W
f=170 GHz => P= 220 W



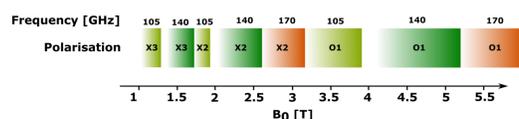
waveguide ohmic losses	0.004 % / 1m
MOU losses of axial offset (2 mm)	0.9 %
MOU losses of tilted (0.2 deg)	1 %
Misalignment losses of axial offset (2 mm)	1. %
Misalignment losses of tilted (0.2 deg)	1.1 %
Miter bend ohmic losses	0.25 % (E plane), 0.07 % (H plane)
Miter bend mode conversion losses	0.07 %
Polarizer ohmic losses	0.5 % (E plane), 0.14 % (H plane)
gap losses (below, pumping tee)	0.008 % (25mm) 0.002 % (2.5mm) 0.2 % (50 mm)

BN disc
d=1.98 mm/2.03 mm, $\tan \delta = 115 \times 10^{-5}$, $\epsilon = 4.7$
f=105 GHz => P= 14 kW, f=140 GHz => P= 18 kW
f=170 GHz => P= 23 kW



ECRH HEATING SYSTEM

The wide range of toroidal magnetic field forces us to compose ECRH as a versatile system with different gyrotron frequencies. Inspired by the experiences from TCV, ASDEX, W7-X, KSTAR

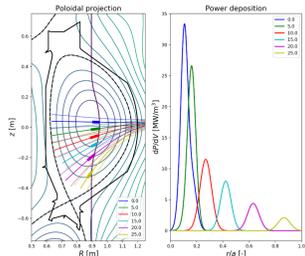


Main goals of ECRH system:

core and off axis heating, impurity management, NTM control, assisted breakdown

First plasma operation $\approx 3T$ and full performance at 5T

140 GHz, O1 mode, 5 T, 2 MA, $1.8 \times 10^{20} \text{ m}^{-3}$



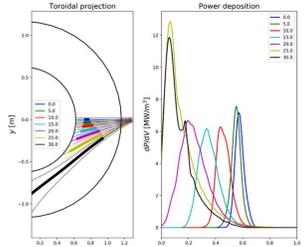
The reference gyrotron:

1 MW power for 1-3 s pulse

Gaussian output fraction > 95%

Cryogen-free technology of magnet, with a cryo-cooler

- 105/140 GHz dual frequency gyrotron
- 170 GHz gyrotron
- 200+ GHz gyrotron (DEMO relevant frequency)

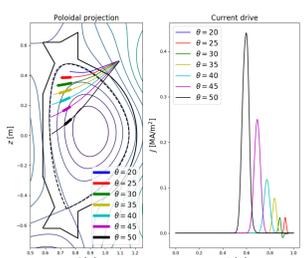


140 GHz, O1 mode, 4.3 T, 1.4 MA, $1.5 \times 10^{20} \text{ m}^{-3}$

Total power delivered to the plasma will be different for each scenario and depends on the available number of gyrotron with adequate frequency.

Toroidal steering is necessary for 140 GHz, O1 at $\approx 4.5 \text{ T}$. With the gyrotron available on the market it is not possible to employ ECRH system during the 5T, high density H mode. ECRH is limited by the cut off density

O-mode: **cutoff density $\approx 2.5 \times 10^{20} \text{ m}^{-3}$**



140 GHz, O1 mode, 4.3 T, 1.4 MA, $1.8 \times 10^{20} \text{ m}^{-3}$

For more details see poster of M. Farnik

	105/140 GHz gyrotron				
	1.2T	2.5 T	3 T	3.5 T	4.5 T
Magnetic field	1.2T	2.5 T	3 T	3.5 T	4.5 T
Mode	105 GHz, X3	140 GHz, X2	105 GHz, O1	105 GHz, O1	140 GHz, O1
Density limit [m^{-3}]		0.8×10^{20}	1.4×10^{20}	1.4×10^{20}	2.5×10^{20}
$p < 0.3$, w/o steering	only 30% absorption				
$p < 0.3$, with steering					
$0.6 < p < 0.9$, w/o steering					
$0.6 < p < 0.9$, with steering					

	170 GHz Gyrotron		
	2.5 T	3 T	5 T
Magnetic field	2.5 T	3 T	5 T
Mode	170 GHz, X2	170 GHz, X2	170 GHz, O1
Density limit [m^{-3}]	3.5×10^{20}	3.5×10^{20}	3.5×10^{20}

STRAY RADIATION

After multiple reflections of the unabsorbed beam from vacuum vessel and plasma, stray microwave radiation builds up. During the flat-top phase, a polarization mismatch of the launched wave is the main source of stray microwave radiation.

Main materials inside vacuum vessel: Inconel 625 and 718, SS 316, Tungsten

Power balance in multi cell model

16 cell for invessel sector + 16 cells for port extension tube

$$(P_{in})_j + \sum_{bordering} p_n A_n = p_j \sum_{bordering} A_n + p_j \sum_{bordering} L_n \rightarrow P_{in}$$

$$L = A_{loss} + \beta A_{wall} + \alpha A_{plasma}$$

$$\hat{B} \cdot \vec{p} + \hat{L} \cdot \vec{p} = \vec{P}_{in} + \hat{A} \cdot \vec{p}$$

