



# Recent Progress on the Electron Cyclotron Emission Diagnostics Development for ITER

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with

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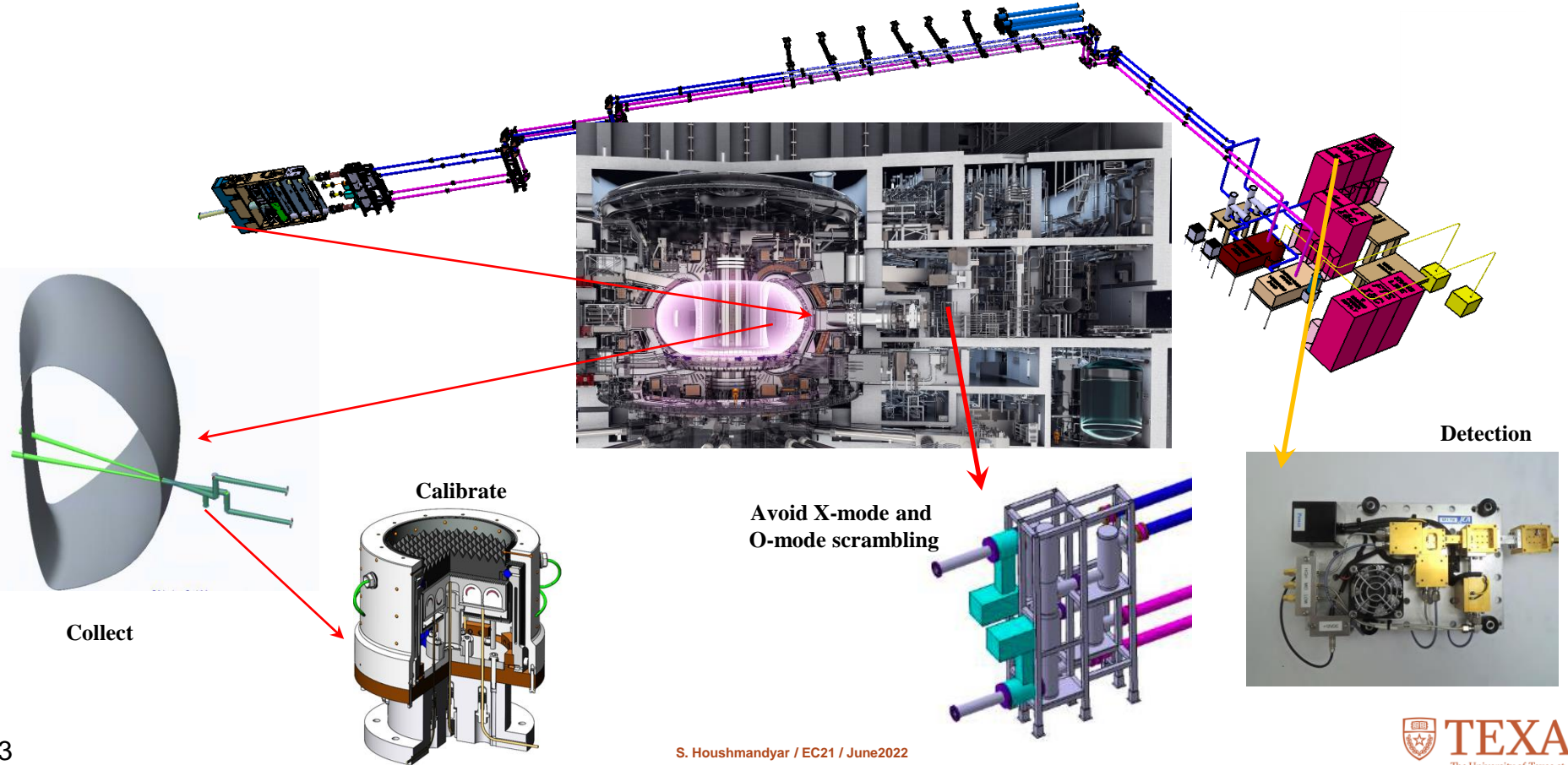
This work is supported PPPL subcontract S013464-C via U.S. DOE Contract No. DE-AC02-09CH11466 with Princeton University.



# ECE Diagnostics are in Final Design Phase, Transitioning to Development

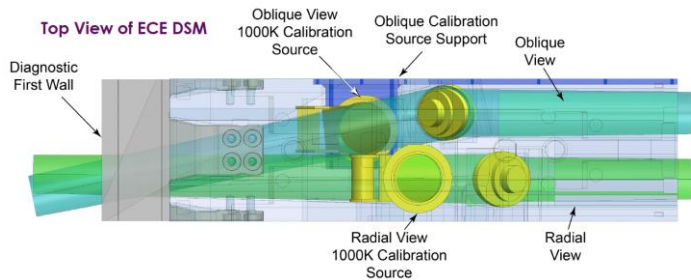
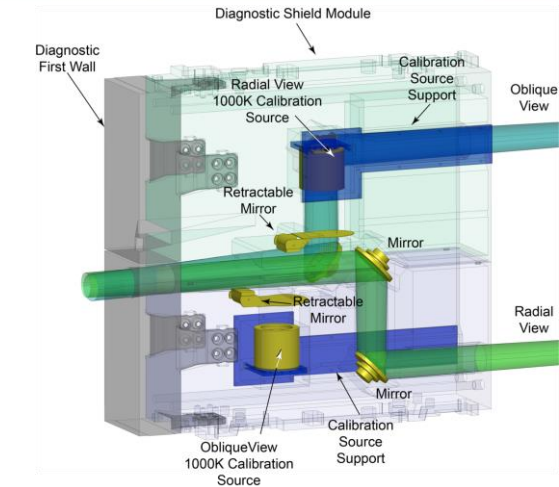
- **Electron Cyclotron Emission (ECE) diagnostics objectives:**
  - Measuring high spatial and temporal resolution electron temperature ( $T_e$ ) and electron temperature fluctuations ( $\delta T_e$ ).
  - Provide temperature profiles to Plant Control System (PCS) for control purposes.
  - Detect Neoclassical Tearing Modes (to PCS), MHD activities and Alfvén Eigen modes.
  - Assess non-thermal electron distributions (via the oblique view).
- **The diagnostics design is a collaboration between Domestic Agencies of United States and India, as well as ITER Organization.**
  - **The efforts in the US-DA are shared with:**
    - The University of Texas at Austin (UT): Front-end optics including hot calibration sources, high frequency radiometer (220 – 340 GHz), performance evaluation.
    - Princeton Plasma Physics Laboratory (PPPL): port integration, shutter actuators, mirror fabrication and fixtures.
  - IN-DA responsible for transmission lines, low frequency radiometer (122 – 230 GHz), Fourier Transform Spectrometers (70 – 1000 GHz), polarization splitter units (PSUs), switch yard, and ECH stray radiation protection system.
  - All parties involved in Instrumentation and Control: software and documentation.

# ITER ECE: The Big Picture

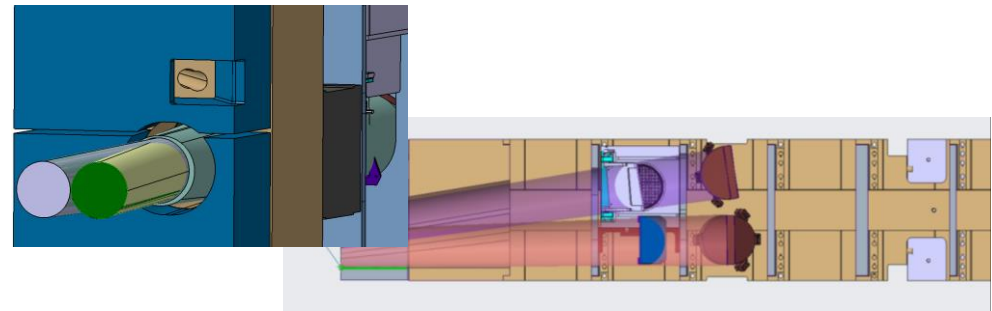
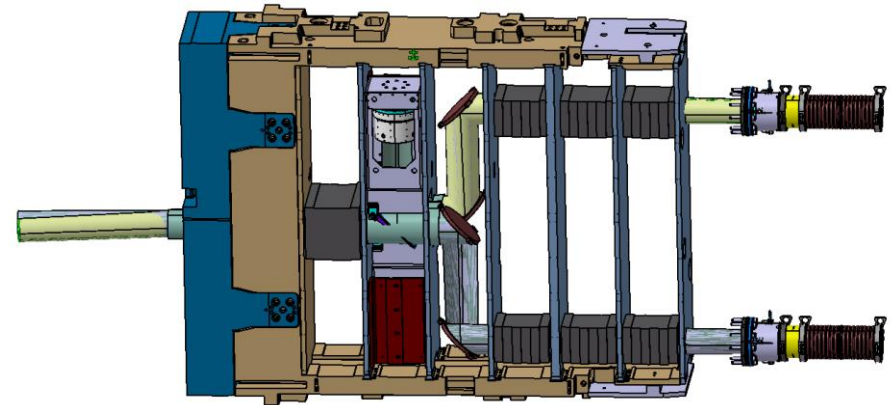


- **Front-end design for the ITER ECE diagnostics.**
  - **Quasi-optical analysis.**
  - **In-situ hot calibration source.**
- **Polarization splitting of X and O modes.**
- **Transmission Line.**
- **Radiometer channel design.**

# Significant changes since 2017 Design of ITER ECE

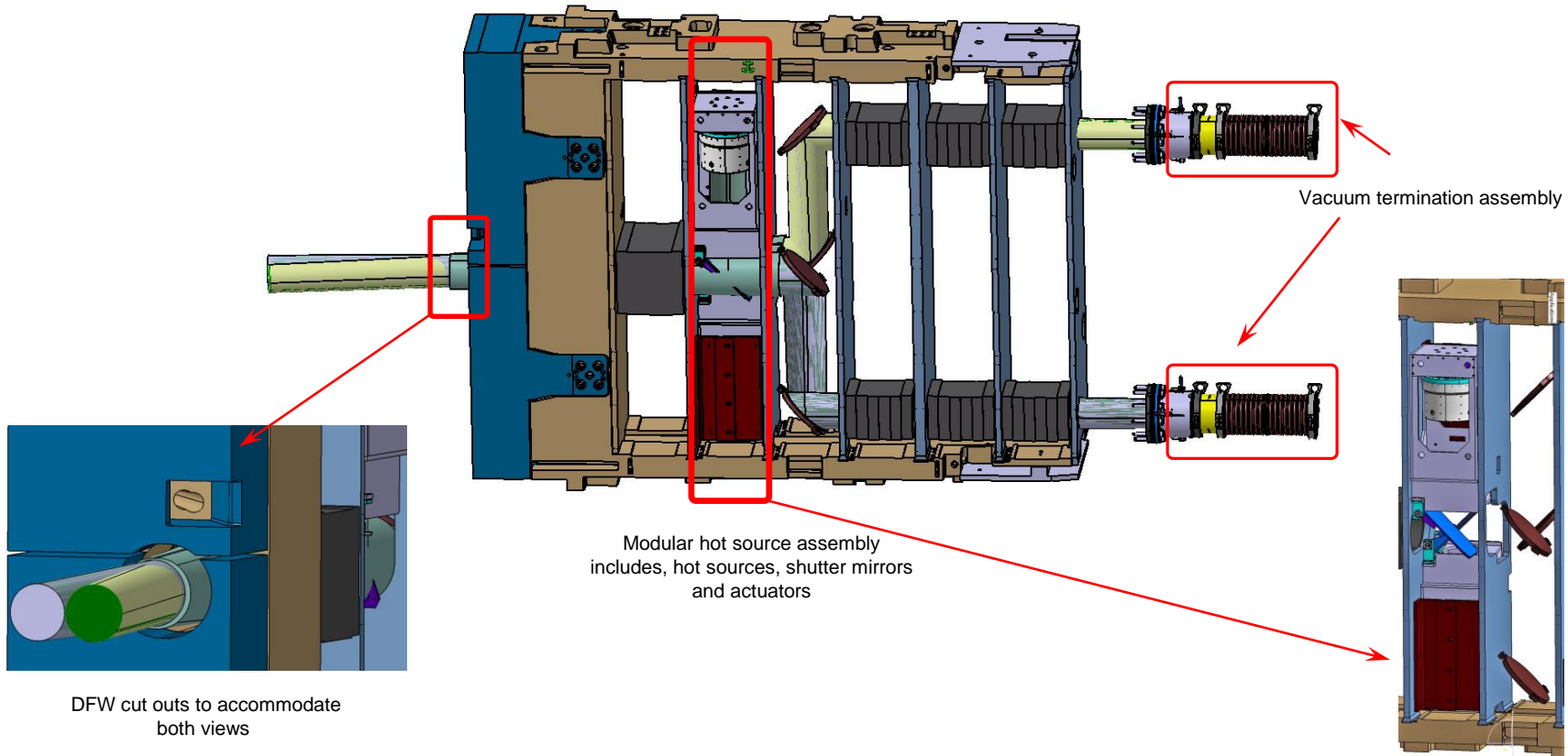


**Pre 2017 design**



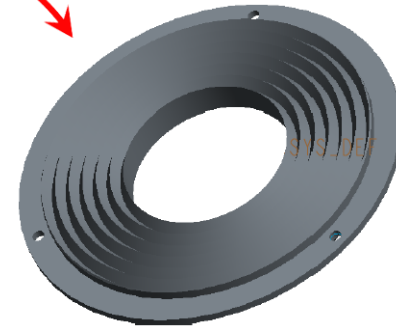
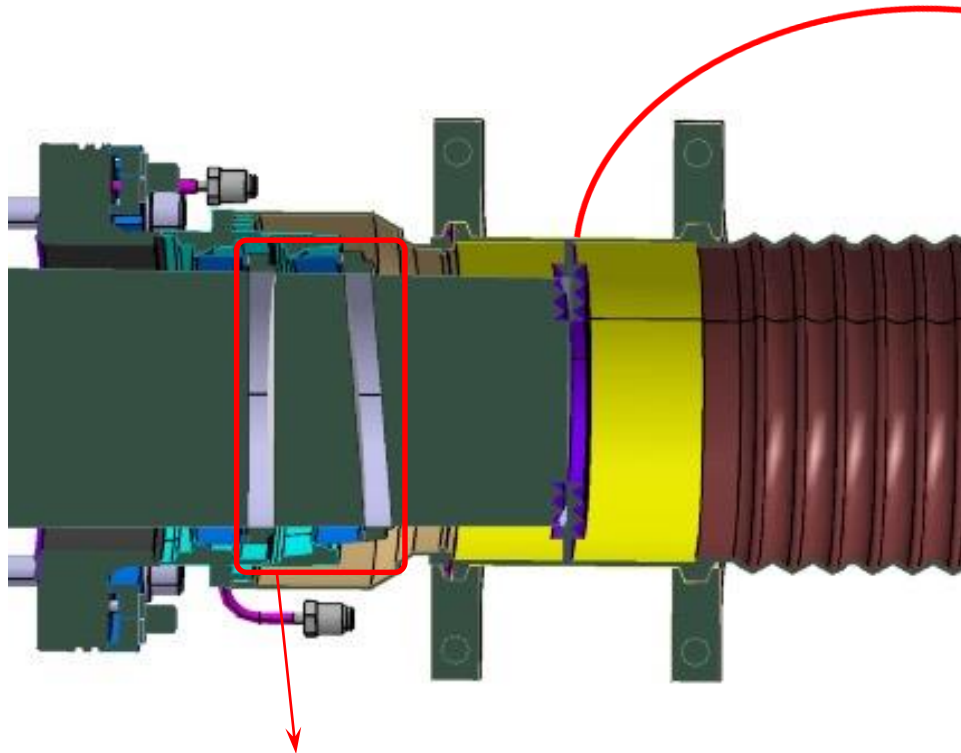
**Current design**

# New front-end design partially driven by the neutron shielding





# Vacuum termination assembly and aperture (point D)



Silicon Carbide (SiC)  
aperture defines the view in  
the plasma, acting as field  
stop. 41.75 mm ID

Window assembly avoids  
interference patterns

*“The large distance from the diagnostic flange to the plasma center ( $> 3$  m) and the large plasma diameter ( $> 6$  m) call for antennas for radiation collection with minimum divergence angles. ... Gauss beam collection optics probably offer the best means of achieving suitable antenna pattern control. ”*

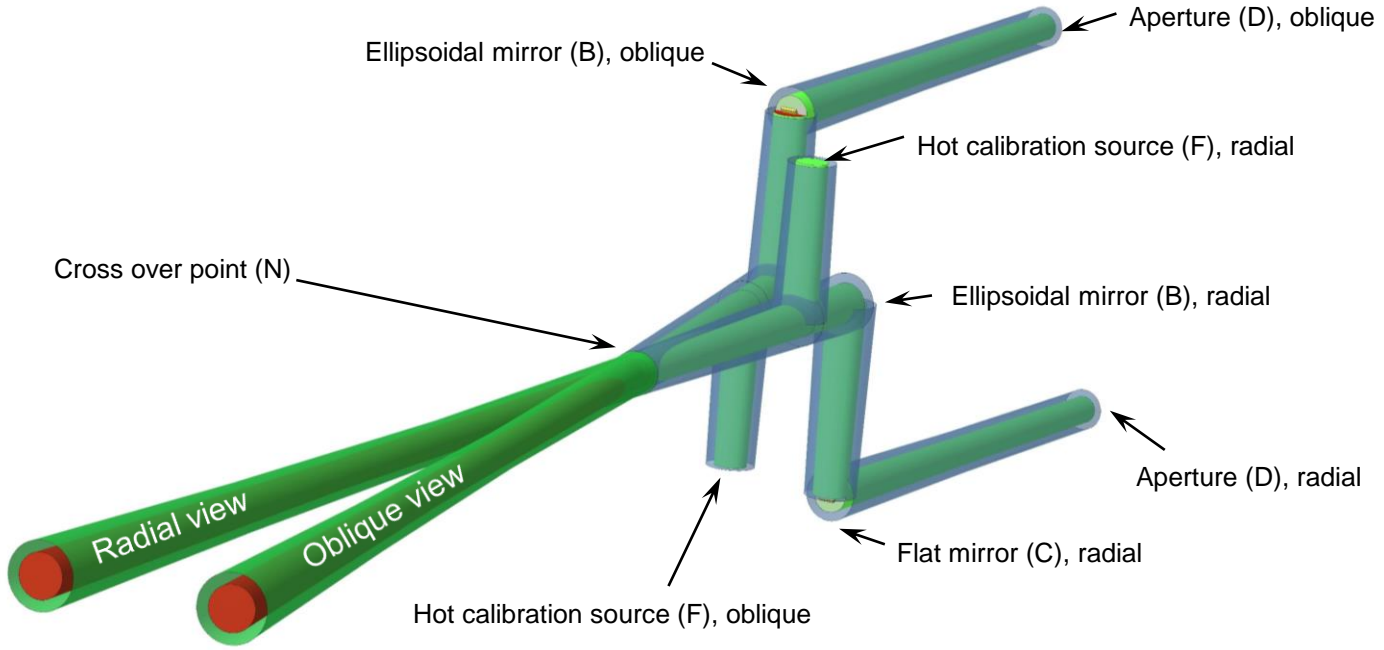
-- Hans J. Hartfuss

Instrumentation of ECE for ITER

Diagnostics for Experimental Thermonuclear Fusion Reactors (1995)



# Gaussian beam calculation for in-vessel optics



- Radial and Oblique Views, 115 GHz
- Modeled using Thomas Keating Gaussian Beam Library

# Gaussian beam calculation for in-vessel optics

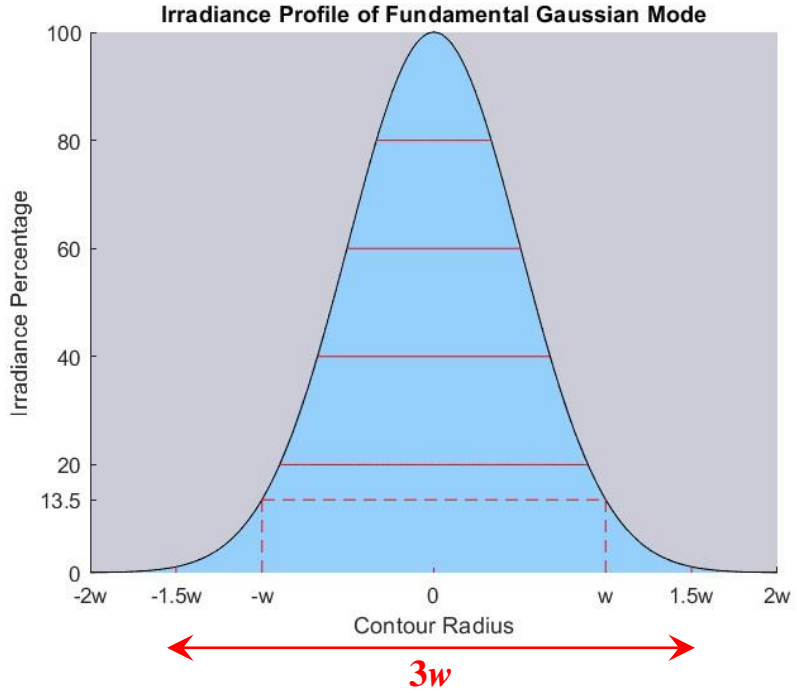
$$w(z) = w_0 \sqrt{1 + \left(\frac{\lambda z}{\pi w_0^2}\right)^2}, \text{ and}$$

$$R(z) = z \left[1 + \left(\frac{\pi w_0^2}{\lambda z}\right)^2\right]$$

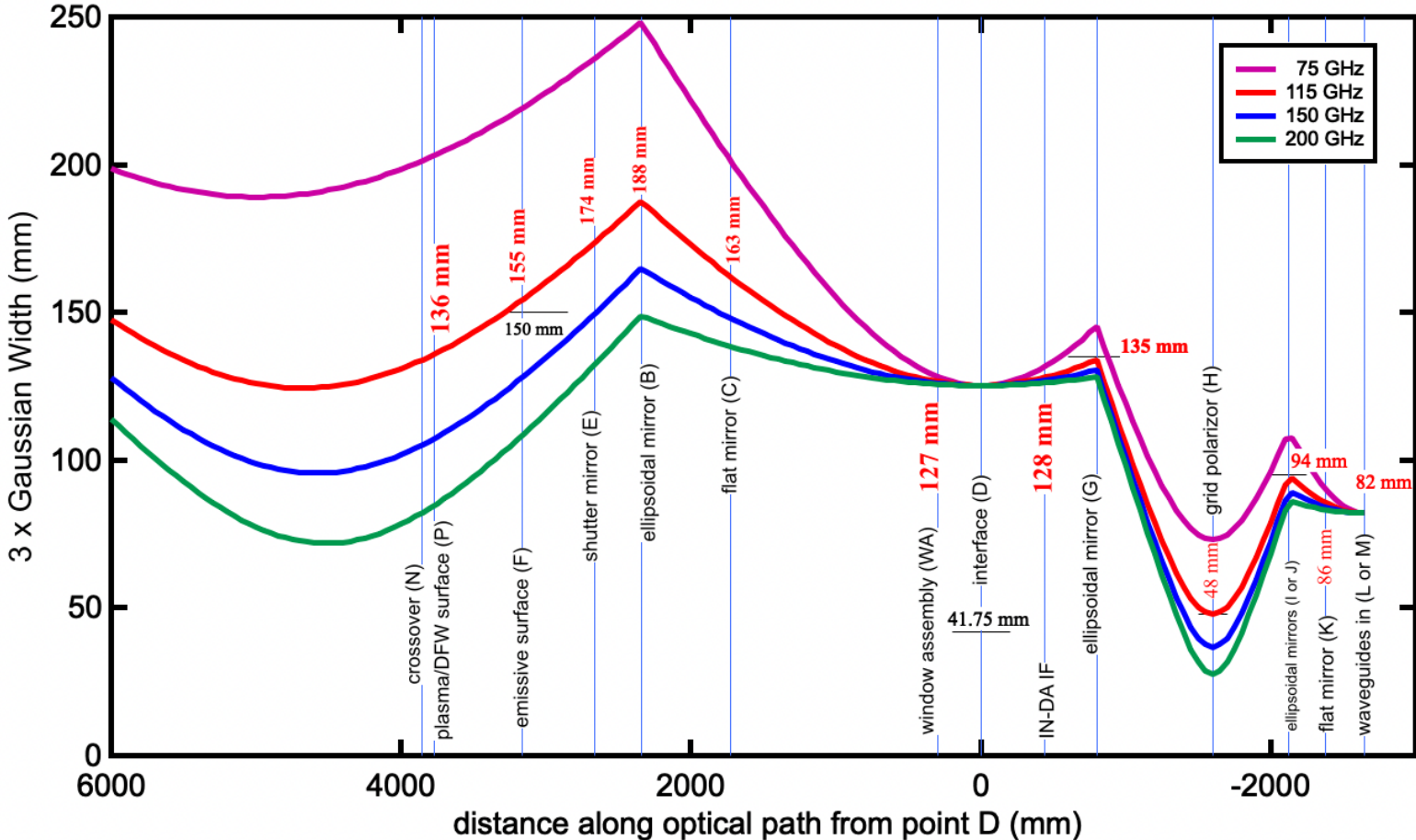
where  $R(z)$  is the curvature of the wave front,  $w_0$  is the aperture's radius at the aperture (D),  $z$  is the length along the beam and  $\lambda$  is beam's wavelength, and  $w_0 = 41.75$  mm.

$$\frac{P}{P_0} = 1 - e^{-\frac{2a^2}{w^2}}$$

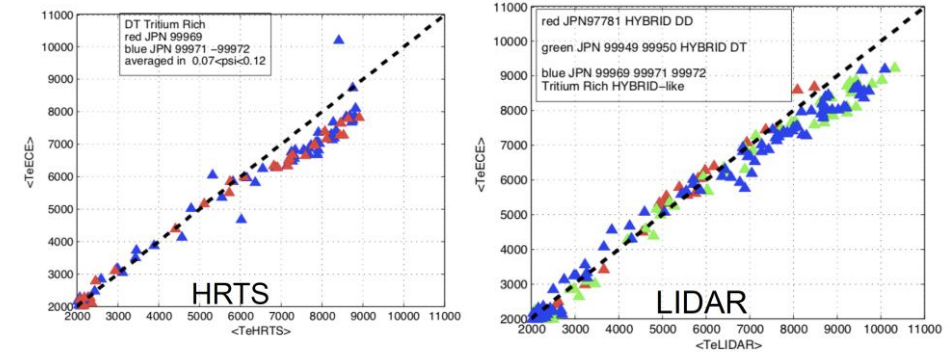
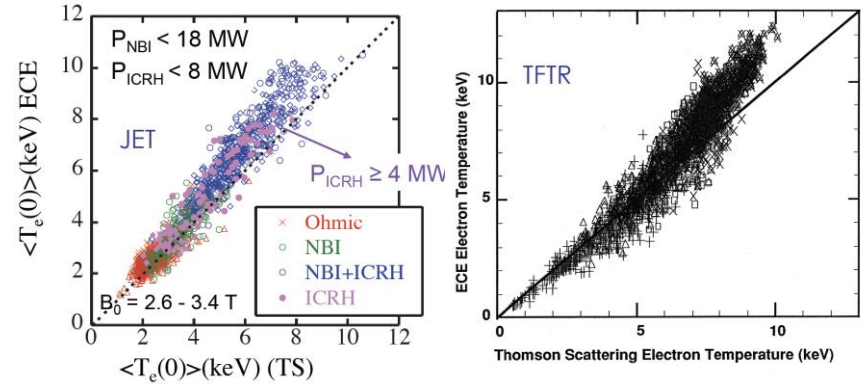
$2w$  is equivalent to 86.5% power throughput  
 $3w$  is equivalent to 98.88% power throughput



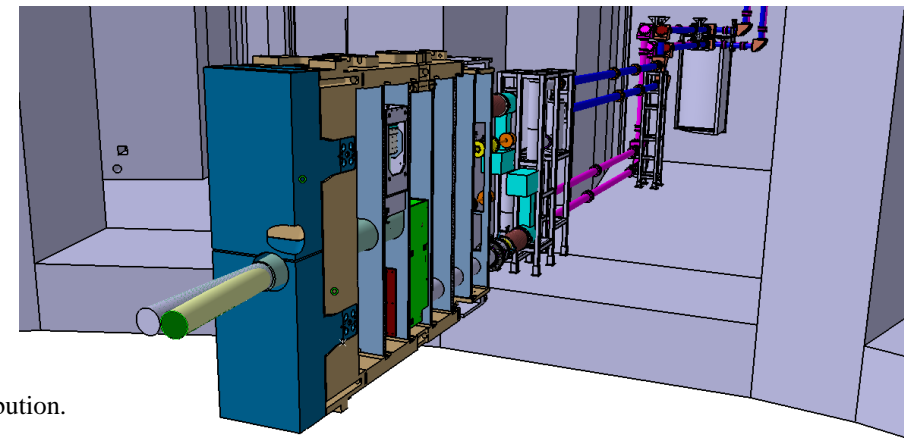
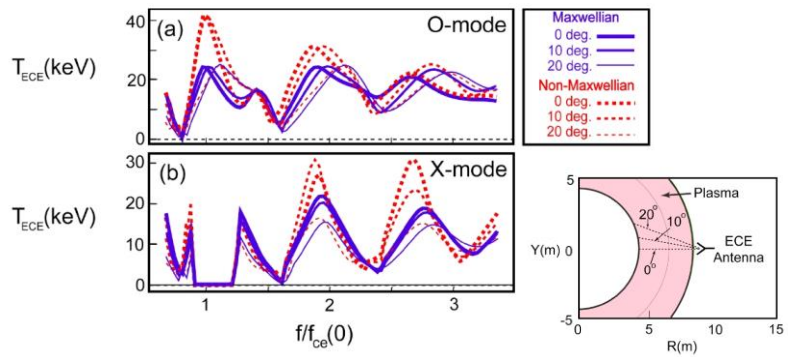
# Viewing volume size for in-vessel optics



# Oblique view will further our understanding of ECE vs Thomson Scattering $T_e$ measurements discrepancies



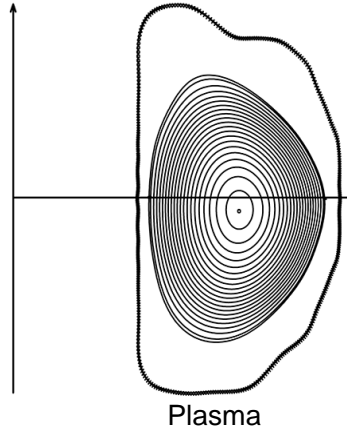
F. Orsitto *et al*, High Temperature Plasma Diagnostic Conference (2022)



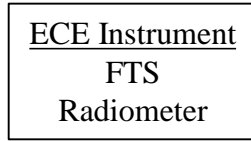
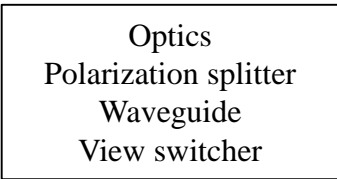
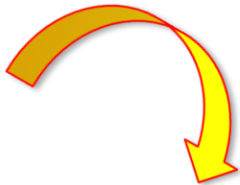
The oblique view can possibly detect non-thermal distribution.

# Hot calibration sources ensure absolute $T_e$ measurements

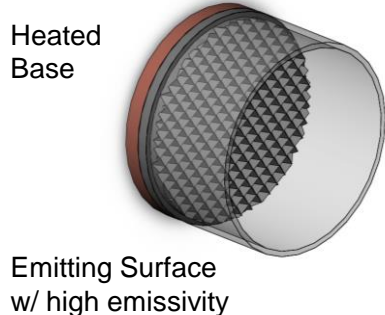
## ECE Measurements



$$I(\nu, R) = \gamma T_e$$



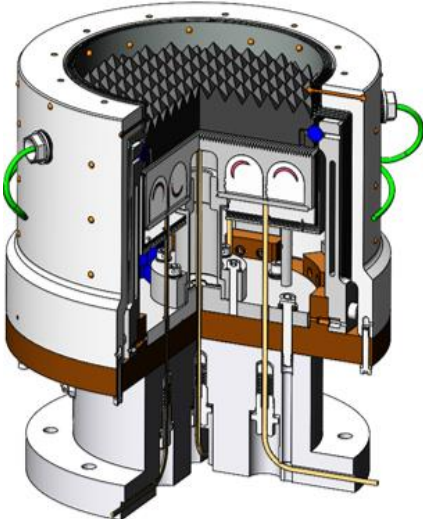
## Hot Calibration Source



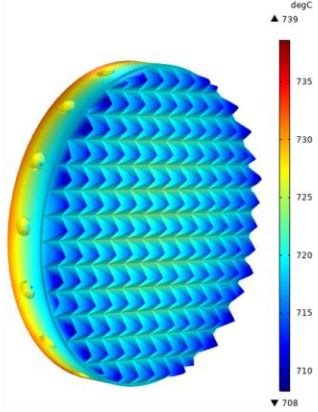
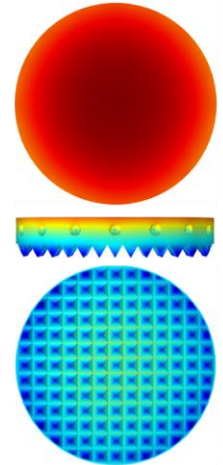
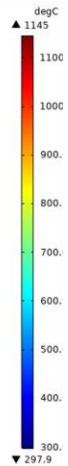
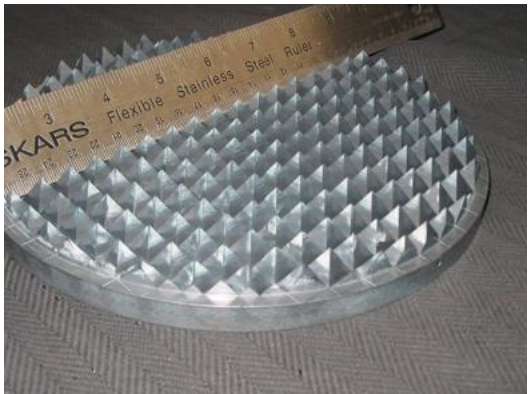
$$I(\nu, T) = \epsilon \frac{2h\nu^3}{c^3} \frac{1}{\exp\left(\frac{h\nu}{kT}\right) - 1}$$



# Hot calibration sources ensure absolute $T_e$ measurements

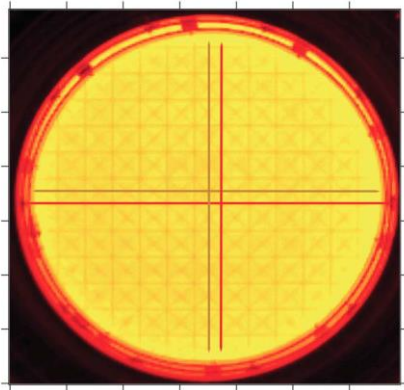
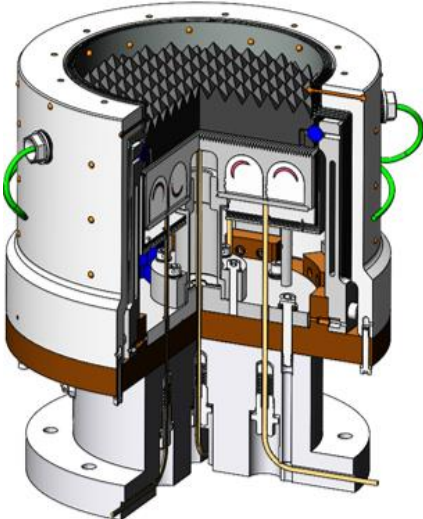


Engineered Hot Source



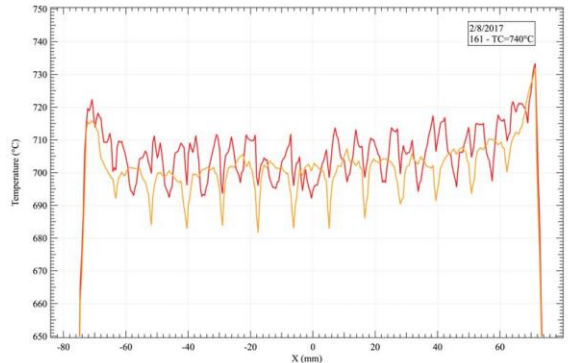


# Prototype hot calibration source achieved a uniform ( $>700\text{ }^{\circ}\text{C}$ ) Blackbody emission

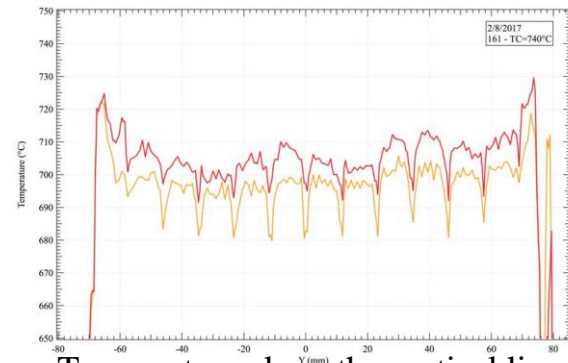


False color IR image  
 $740\text{ }^{\circ}\text{C}$

## Temperature Uniformity



## Temperature along the horizontal lines



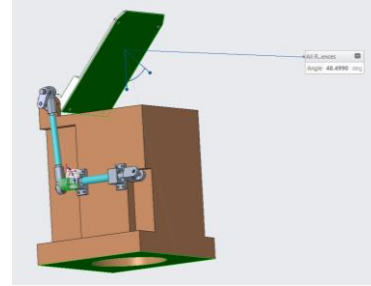
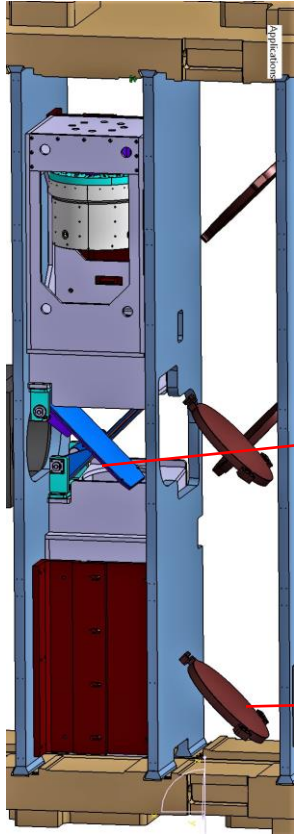
## Temperature along the vertical lines



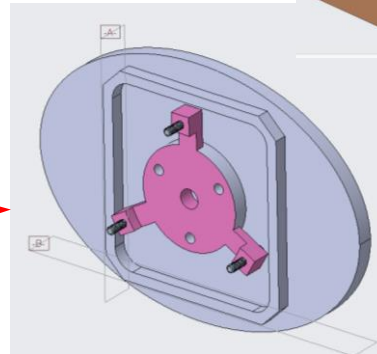
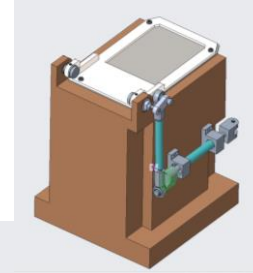
# Hot source testing

- Status
  - Conducted over 2000 hours of high temperature testing
    - Selected one of three alternatives
  - Encapsulated molybdenum heater successfully:
    - Heated SiC emitter to  $> 700\text{ }^{\circ}\text{C}$
    - Achieved emitter surface temperature uniformity  $< 10\text{ }^{\circ}\text{C}$
    - Operated in high vacuum:  $\sim 10^{-8}$  Torr
    - Demonstrated stable short term (24 hours) operation
    - Used feedback control so longer times are likely no problem
  - Outgassing test met ITER requirements
- Design revised following peer review
  - Primary change: removal of alumina potting due to swelling induced by neutron irradiation
- Next challenges to complete the new design
  - Longevity test for new design
  - Vibration test using ITER loads
  - Steam testing (VV ICE)

# Shutter mirrors in front of hot sources allow remote switching between viewing the plasma and the hot sources



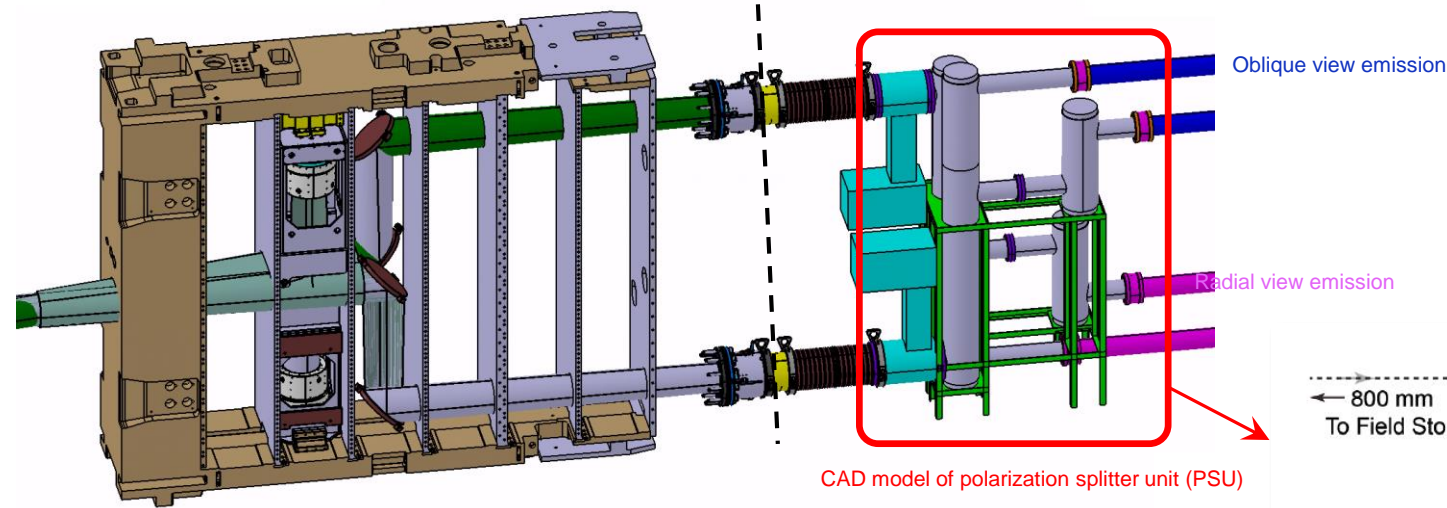
Shutter assembly



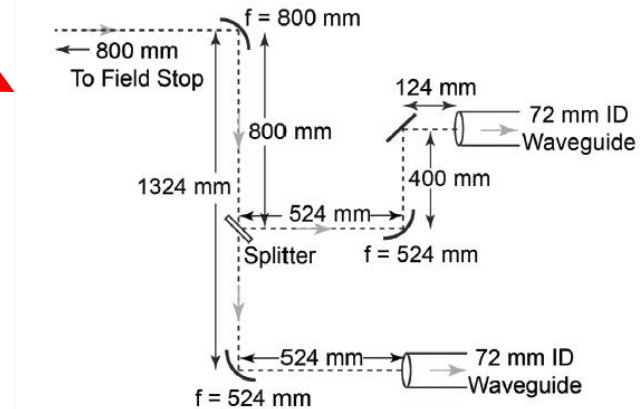
Ellipsoidal mirror



# Polarization splitter unit separates modes prior to waveguides, avoids scrambling modes in waveguides



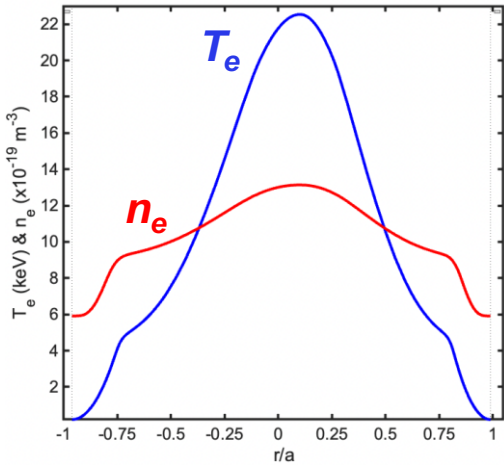
CAD model of polarization splitter unit (PSU)



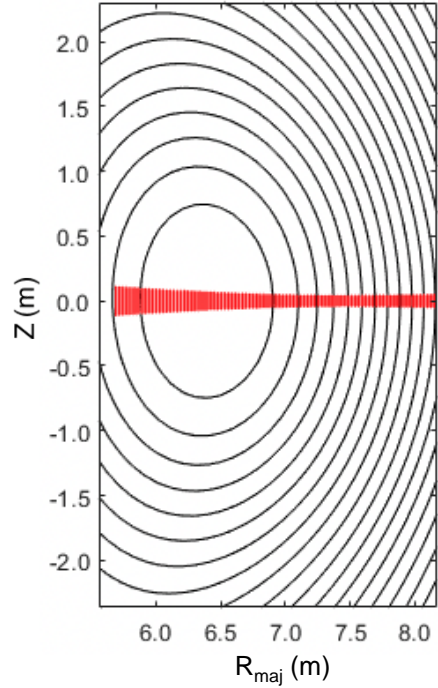
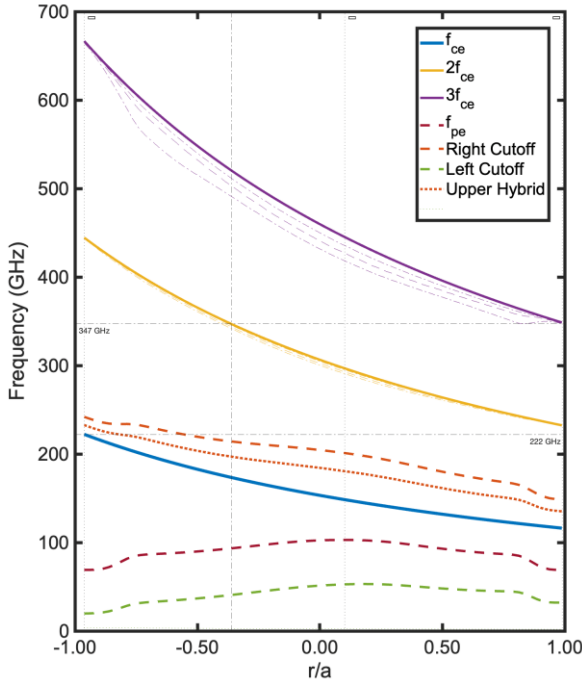
- Support structure design for the Polarization Splitter Unit was updated.
- Preliminary studies were carried out to assess the need of Displacement Compensation System.

# Radiometer channel design

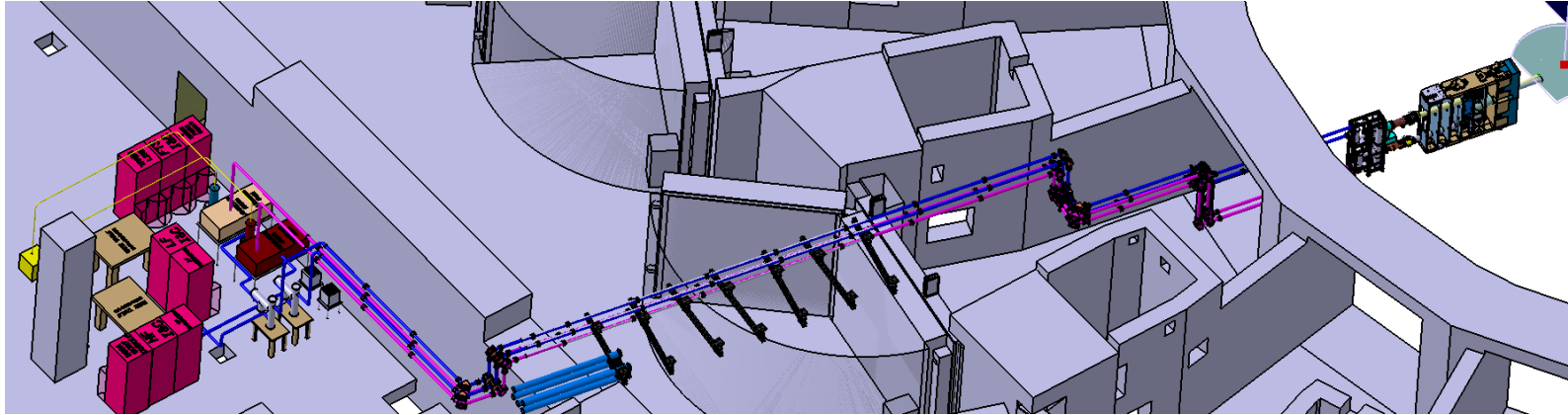
- 2<sup>nd</sup> harmonic is optically thick
- $P = k T_e \Delta f$  leads to temperature measurement
- Complications due to relativistic broadening for ITER plasmas



\* ITER scenarios used to guide the design

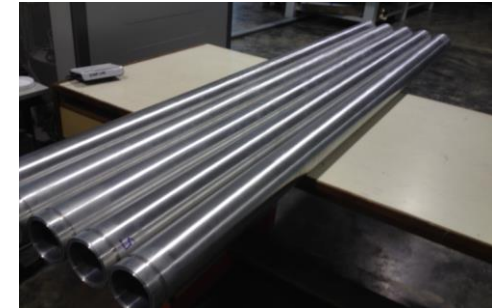


# Transmission Line



- 43 meters long
- Desire loss less than:
  - 15 dB for 70 - 400 GHz
  - 22 dB for 400 – 1000 GHz
- Waveguide and not QO

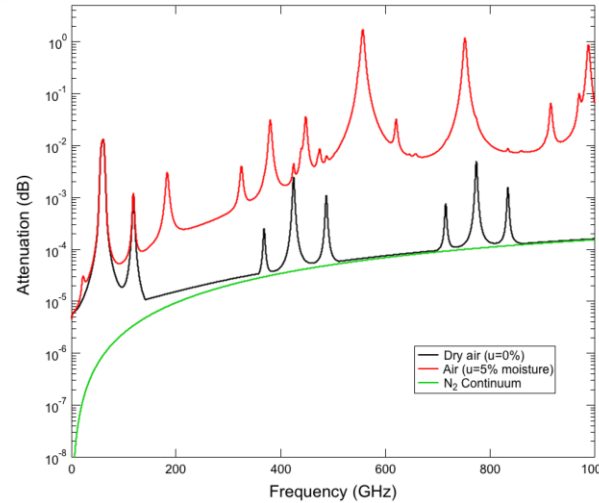
Parameter	Specifications
Waveguide Material	Aluminium, 6061 T6 Alloy
Inner Diameter of Waveguide (mm)	72 ±0.05
Outer Diameter of tube (mm)	88±0.5
WG Inner surface finish	7.5 micron Ra
Ellipticity, WG tube inner surface [mm]	<0.1 mm



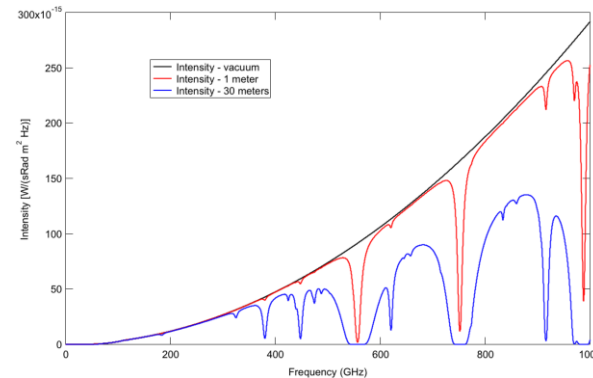
# The transmission line is purged to minimize the microwave attenuation

## Conduct Microwaves to Instruments

- ☐ Minimize microwave attenuation
- ☐ Consistent with lab safety
  - Contain radiation hazard if there is a tritium leak
  - Avoid asphyxiation hazard due to purge gas



*Attenuation  
due to  
Purge*



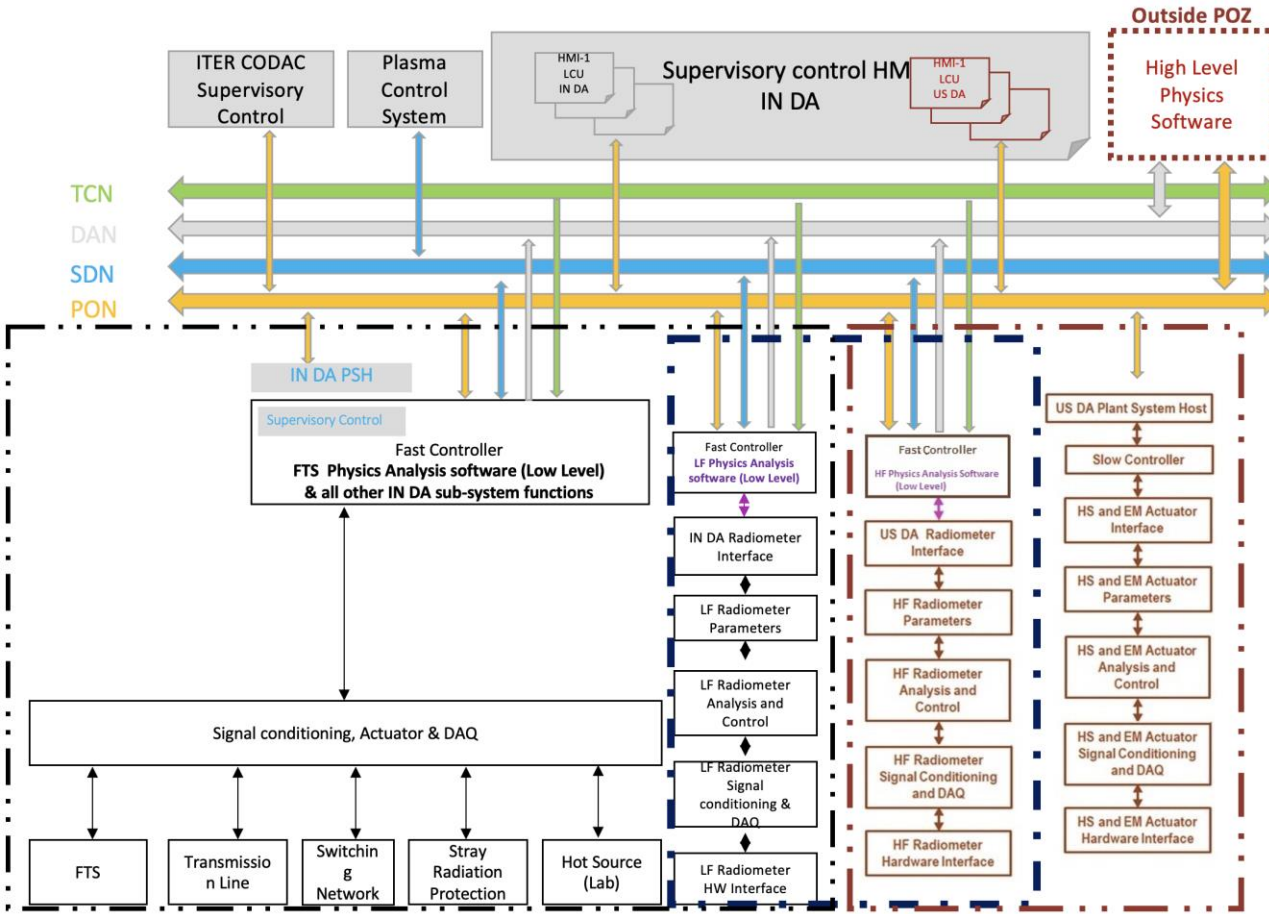
*Typical  
Power  
Transmission*



# I&C Hardware Architecture

**IN-DA**  
 Created I&C hardware architecture.  
 Responsible for local control cubicle.

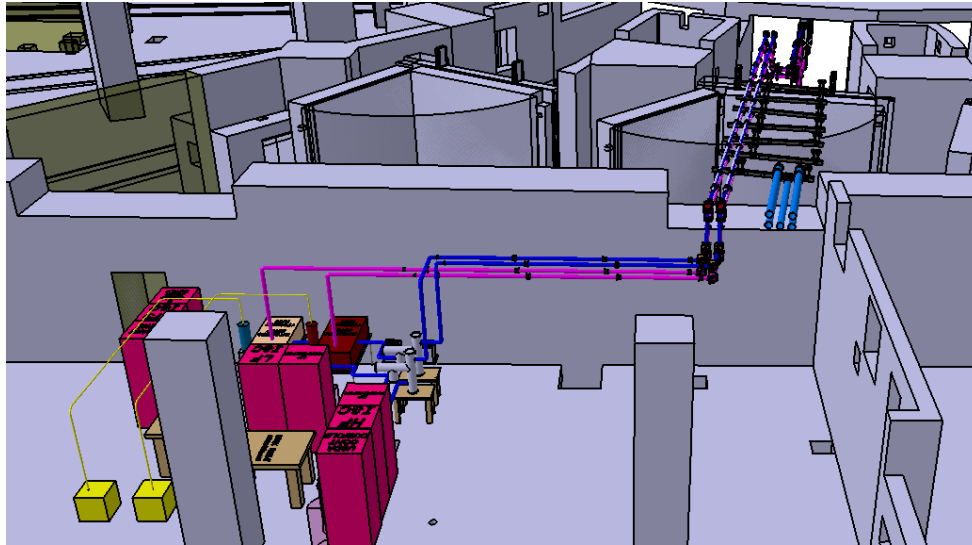
**US-DA**  
 Designs radiometer cubicles  
 Hot source control cubicles.



**Outside POZ**  
 High Level  
 Physics  
 Software



# Diagnostics Hall Layout

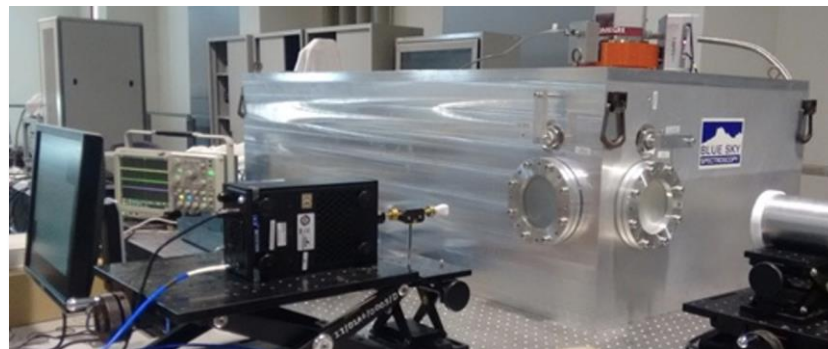
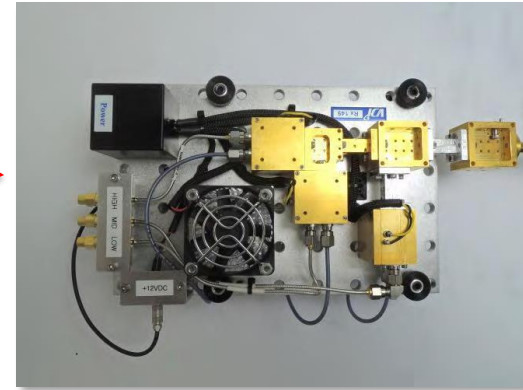


- Detect the EC emission.
- Select view and polarization for the experiment, then feed to instrument.
- Digitize the emission.
- Send profile and NTM information to PCS.
- Send complete data to data archive.
- IN-DA design of stray radiation (from ECH) sensor for ITER ECE Diagnostic was completed (next talk).

Instruments	Quantity
Low Freq Radiometer	1
High Freq Radiometer	1
FTS	2
Power Splitter	2
Hot Source	2
Working Table	2
Cryo-Compressor FTS	2
Cubicles	10

# Diagnostics Hall Layout: Instruments

- The detection instruments are modest evolutions from existing instruments
- Two Radiometers.
  - High Frequency, 220 – 340 GHz  
Fielded on C-Mod and built prototype with improved reliability which is under test at DIII-D
  - Low Frequency 122 – 230 GHz  
Conventional frequency range
- Two FTS
  - Wide bandwidth 70-1000GHz



## Components have been the focus

- **Front end optics.**
  - **Design is complete.**
  - **It's a flexible design: Easily modified during port integration**
- **Radiometers**
  - **Similar to radiometer UT fielded for C-Mod, a 5.4 T tokamak**
  - **Prototype constructed to improve reliability: Under test**
- **Polarization Splitter Unit and transmission line: Prototyped**
- **Hot source (In-situ operation required a novel design)**
  - **Risk reduced by exhaustive testing (in progress) & painstaking design (continuing)**

## Now must put it all together and make it work

- **Port integration: In progress**
- **Control Cubicles: Design underway, informed by prototyping**
- **Actuators for in-vessel components: Starting soon**
- **Fixturing for in-vessel optics: In progress**