

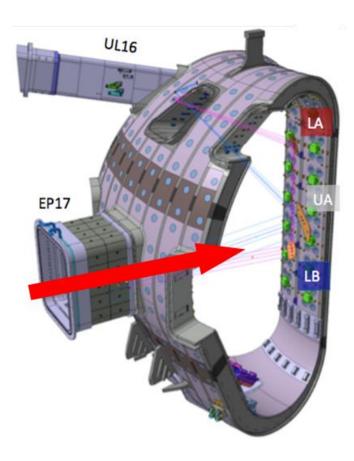
University of Stuttgart

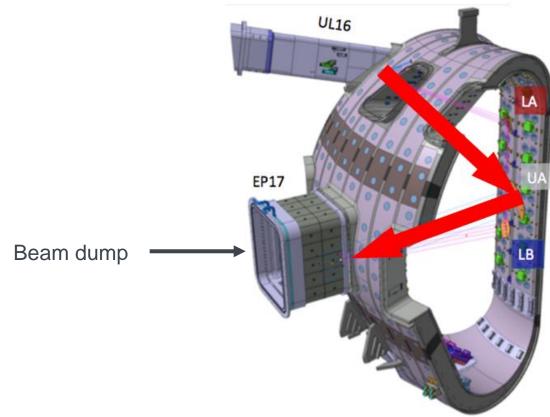
Institute of Interfacial Process Engineering and Plasma Technology

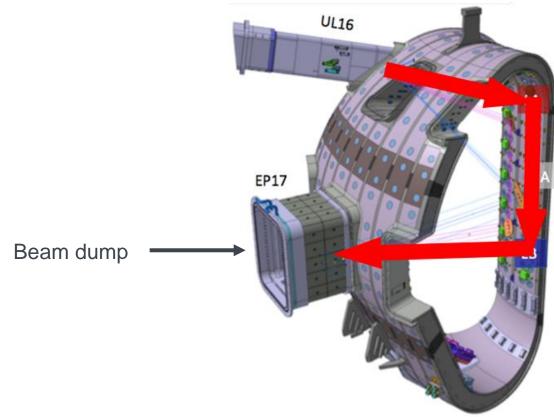
Calculations for the optical system for the first ITER plasma

B. Plaum, M. Preynas, M. Choe

- For the breakdown of the first ITER plasma, the equatorial launcher will not be installed yet.
- Therefore, the MW-beams from the upper launcher will be redirected towards the resonance with a dedicated optics using in-vessel mirrors.
- The design was analysed using the PROFUSION tools



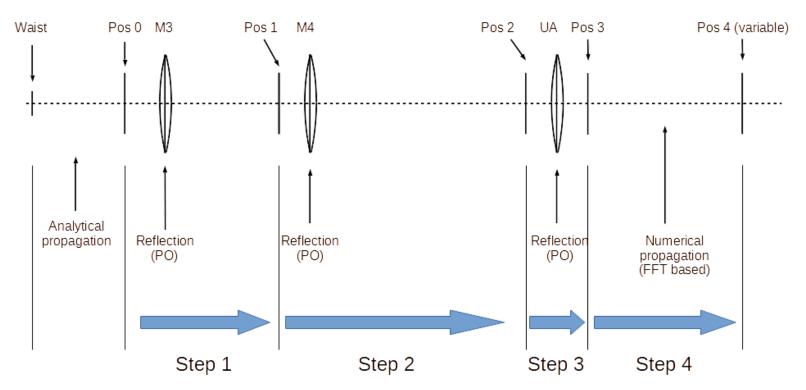




Calculation methods

- Propagation from the start position to the first mirror: **Gaussian Optics** with analytical formulas
- Reflection at the mirrors: **Physical Optics** solver (parallelized to run on 40 CPU cores)
- Propagation after the last mirror: **FFT-Propagation** (plane wave decomposition)
- All calculations were done in vacuum

Calculation scheme (U-Beams)



Physical optics solver

• Calculate the currents in the mirror surface from the incident magnetic field:

 $\vec{J} = 2\vec{n} \times \vec{H}_i$

• Calculate the radiated magnetic field from the currents in the mirror:

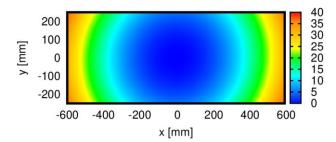
$$\vec{H}_r = \iint (-jk - \frac{1}{R}) \cdot \vec{J} \times \frac{\vec{R}}{R} \frac{e^{-jkR}}{4 \pi R} dy dx$$

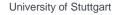
- Very accurate method, which considers:
 - Mode conversion due to non perpendicular incidence
 - Cross polarization effects due to the reflection of straight field lines on a curved surface
 - **Beam truncation** effects due to the limited mirror size, even for irregular (numerically given) shapes

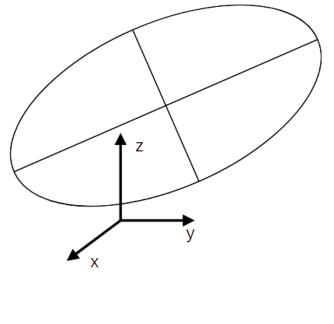
University of Stuttgart

Discretization of the mirror surfaces

- The mirrors are given in terms of ellipsoid-, cylinder-, or hyperboloid-parameters
- For the PO solver we need xyz-Coordinates in a mirror local coordinate system
- Finding the z-coordinate is equivalent to finding the intersection of a line with the surface → no analytical solution
- An iterative method was developed, which starts with 2 points (one above and one below the mirror surface)
- Just a few iterations needed for subatomic precision



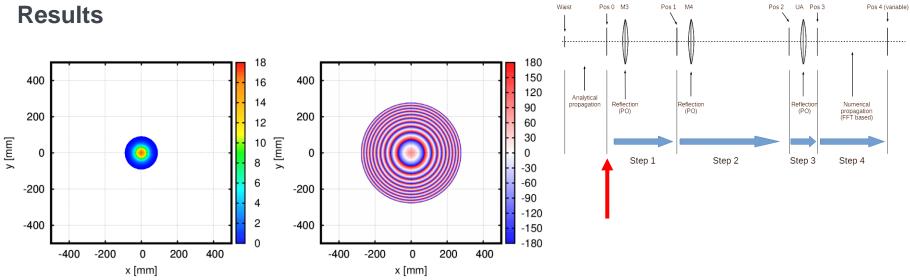


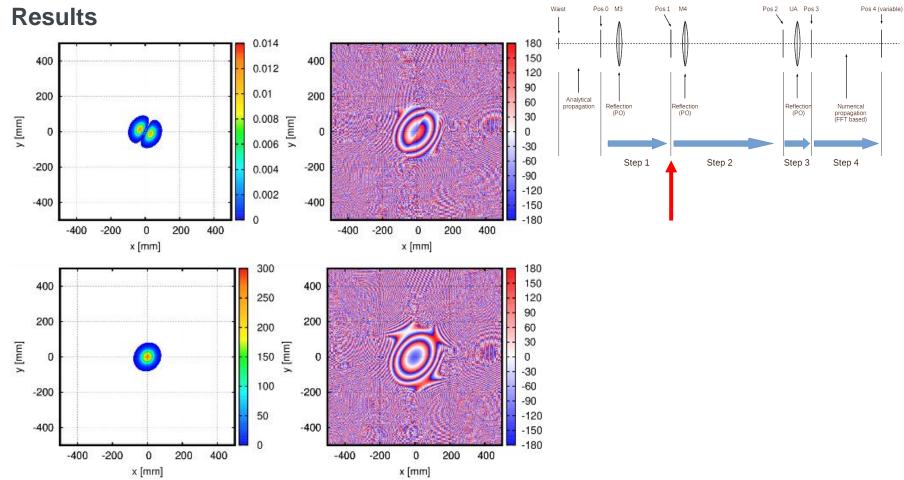


Choice of the coordinate systems

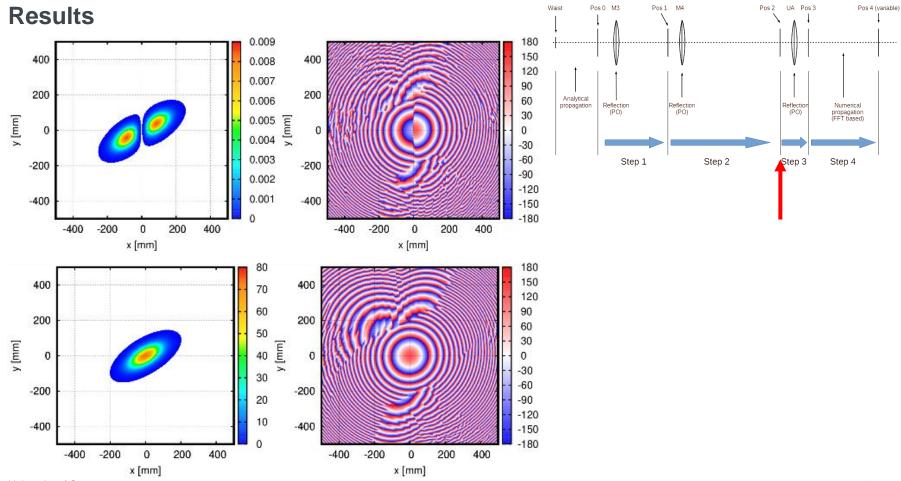
- For beam-local coordinate systems:
 - **Z-axis** is always parallel to the beam axis and points in the **propagation direction**
 - Y-axis is parallel to the desired polarization direction of the E-field
 - For a perfect linear polarization, the x-component is zero
 - Advantage: The cross-polarization (≈ 300W) can be distinguished from the copolarization (1 MW)
- Mirror local systems:
 - **Z-axis** is always the mirror normal at the incident point of the beam axis
 - X- and Y-axes are arbitrary
- All coordinates were provided in TGCS @ OT (Torus Global Coordinates @ Operating Temperature)
 University of Stuttgart

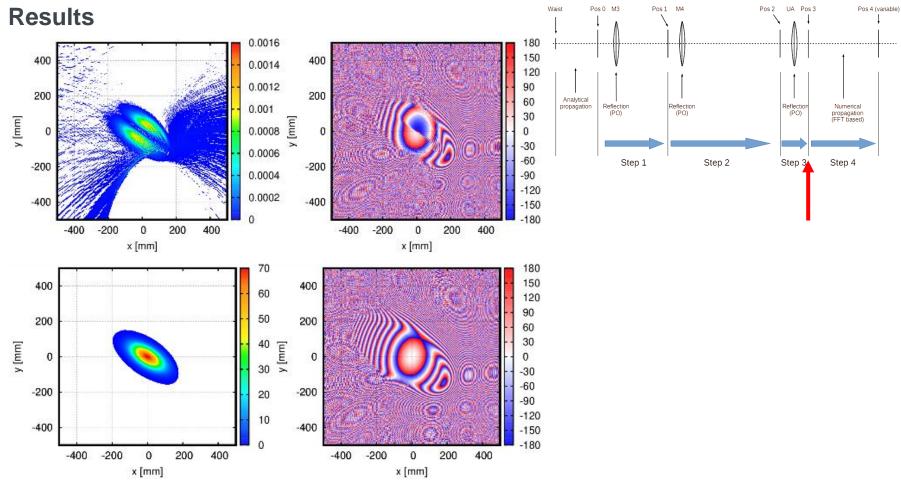
Results



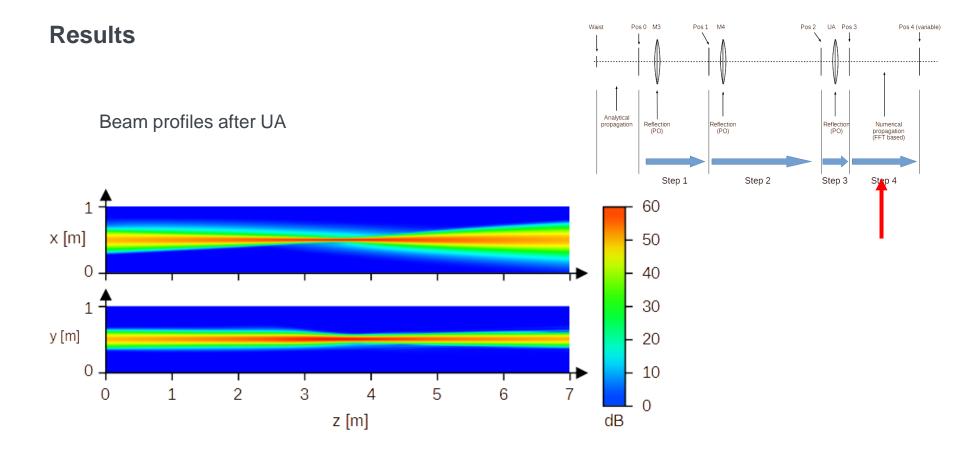


University of Stuttgart

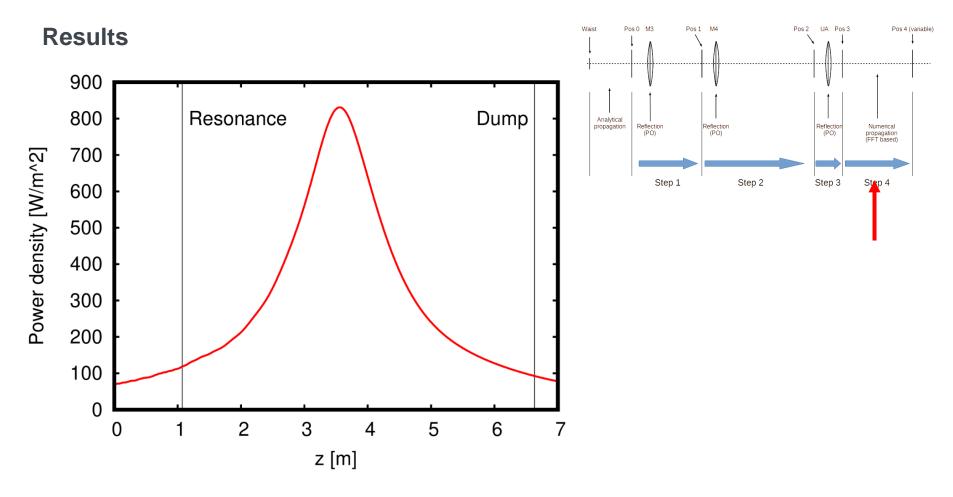




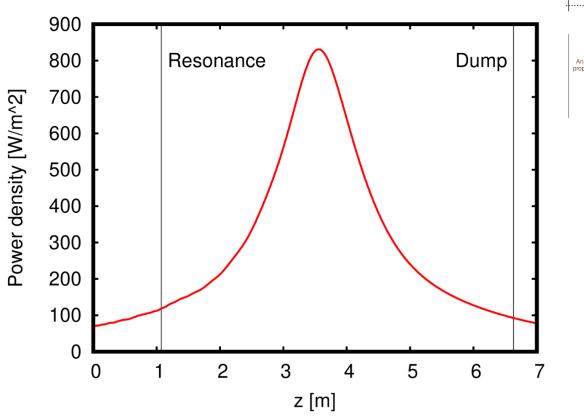
University of Stuttgart

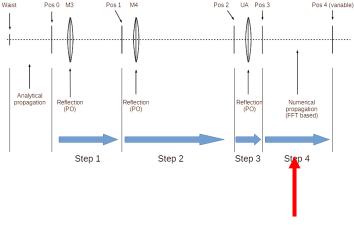


University of Stuttgart



Results

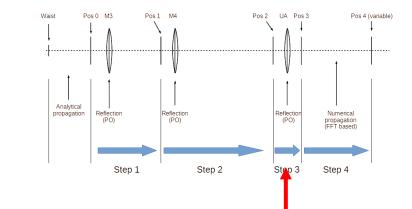


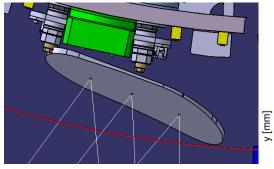


Maximum offset in the beam dump (after 3 mirrors and > 13 m propagation):

1.702 mm







200

100

-100

-200

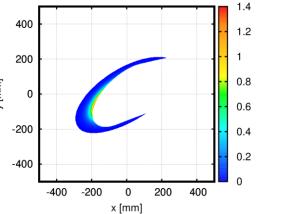
0

-600

-400

-200

y [mm]



200

0 x [mm] 400

600

0.6

0.5

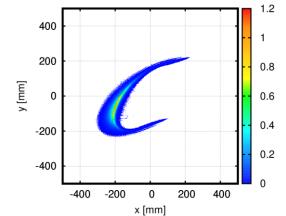
0.4

0.3

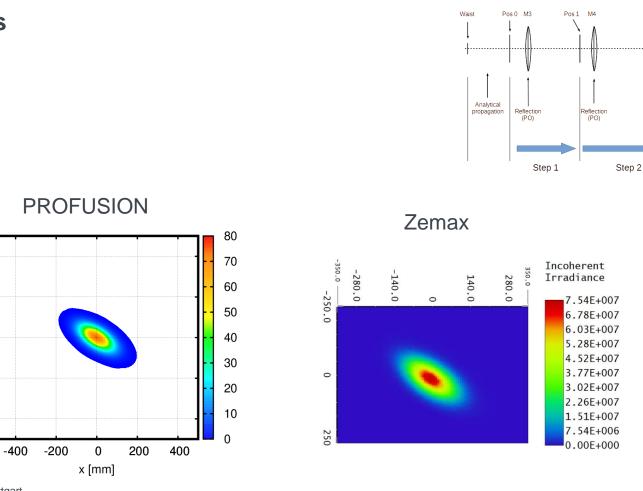
0.2

0.1

0



Results



400

200

0

-200

-400

y [mm]

Pos 2

UA Pos 3

Reflection (PO)

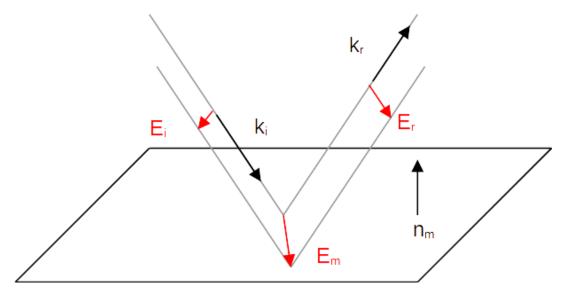
Step 3

Pos 4 (variable)

Numerical propagation (FFT based)

Step 4

Tracking the polarisation



- The polarization plane of a beam is defined by the E-vector and the k-vector in the beam axis
- The projected E-field E_m on the mirror is obtained by intersecting the polarization plane with the mirror (assumed locally flat)
- Simple rule: E_m is the same for the incident and reflected beam

Tracking the polarisation

Normal vector n_i of the incident polarisation plane:

$$\vec{n}_i = \vec{E}_i \times \vec{k}_i$$

Projected E-field E_m on the mirror: $\vec{E}_m = \vec{n}_i \times \vec{n}_m = (\vec{E}_i \times \vec{k}_i) \times \vec{n}_m$

Normal vector n_r of the reflected polarisation plane: $\vec{n}_r = \vec{E}_m \times \vec{k}_r = ((\vec{E}_i \times \vec{k}_i) \times \vec{n}_m) \times \vec{k}_r$

Electric field of the reflected beam:

$$\vec{E}_r = \vec{n}_r \times \vec{k}_r$$

$$\vec{E}_r = (((\vec{E}_i \times \vec{k}_i) \times \vec{n}_m) \times \vec{k}_r) \times \vec{k}_r)$$

Conclusions

- The optics system for the ITER plasma was modelled with the PROFUSION tools
- The code was extended to support irregular mirror contours and polarization tracking
- The design was confirmed, no major disagreements or other obstacles were identified
- Final analysis and comparison with Zemax to be done for the current version of the optical design



University of Stuttgart Institut für Grenzflächenverfahrenstechnik und Plasmatechnologie

Thank you!



Burkhard Plaum

e-mail burkhard.plaum@igvp.uni-stuttgart.de phone +49 (0) 711 685-62174 www.igvp.uni-stuttgart.de

University of Stuttgart Institute of Interfacial Process Engineering and Plasma Technology Pfaffenwaldring 31, D-70569 Stuttgart